



US009188836B2

(12) **United States Patent**
Aoshima et al.

(10) **Patent No.:** **US 9,188,836 B2**
(45) **Date of Patent:** **Nov. 17, 2015**

(54) **SHUTTER DEVICE AND IMAGE PICKUP APPARATUS INCLUDING SHUTTER DEVICE**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.

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(21) Appl. No.: **14/538,055**

(22) Filed: **Nov. 11, 2014**

(65) **Prior Publication Data**

US 2015/0131986 A1 May 14, 2015

Primary Examiner — W B Perkey

(74) Attorney, Agent, or Firm — Canon U.S.A., Inc. IP Division

(30) **Foreign Application Priority Data**

Nov. 14, 2013 (WO) PCT/JP2013/080757

(57) **ABSTRACT**

When a stepping motor is used as a driving source for a shutter device, if the stepping motor loses synchronization because of variations in load during driving or the like, it becomes unable to rotate a driving ring at that time, and this disables an exposure operation. In a first zone where a driven member is driven, but a light shielding member remains in a closed state or an open state, the motor drives the driven member in open-loop driving mode. In a second zone where the driven member is driven, and thus the light shielding member moves to the closed state or the open state, the motor drives the driven member in feed-back driving mode.

(51) **Int. Cl.**

G03B 9/08 (2006.01)

G03B 9/10 (2006.01)

G03B 7/00 (2014.01)

G03B 9/36 (2006.01)

(52) **U.S. Cl.**

CPC .. **G03B 9/10** (2013.01); **G03B 7/00** (2013.01);
G03B 9/36 (2013.01)

(58) **Field of Classification Search**

CPC G03B 9/10; G03B 7/093

See application file for complete search history.

14 Claims, 17 Drawing Sheets

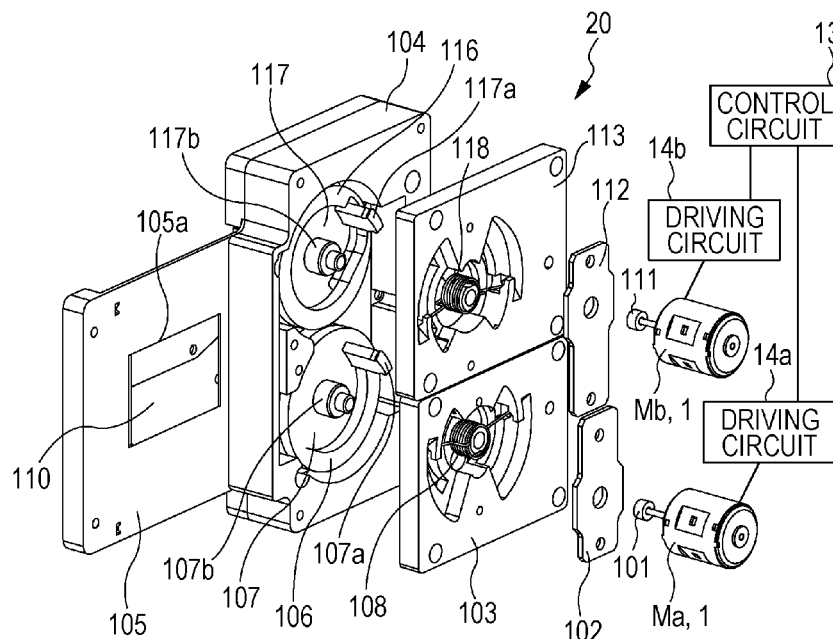


FIG. 1A

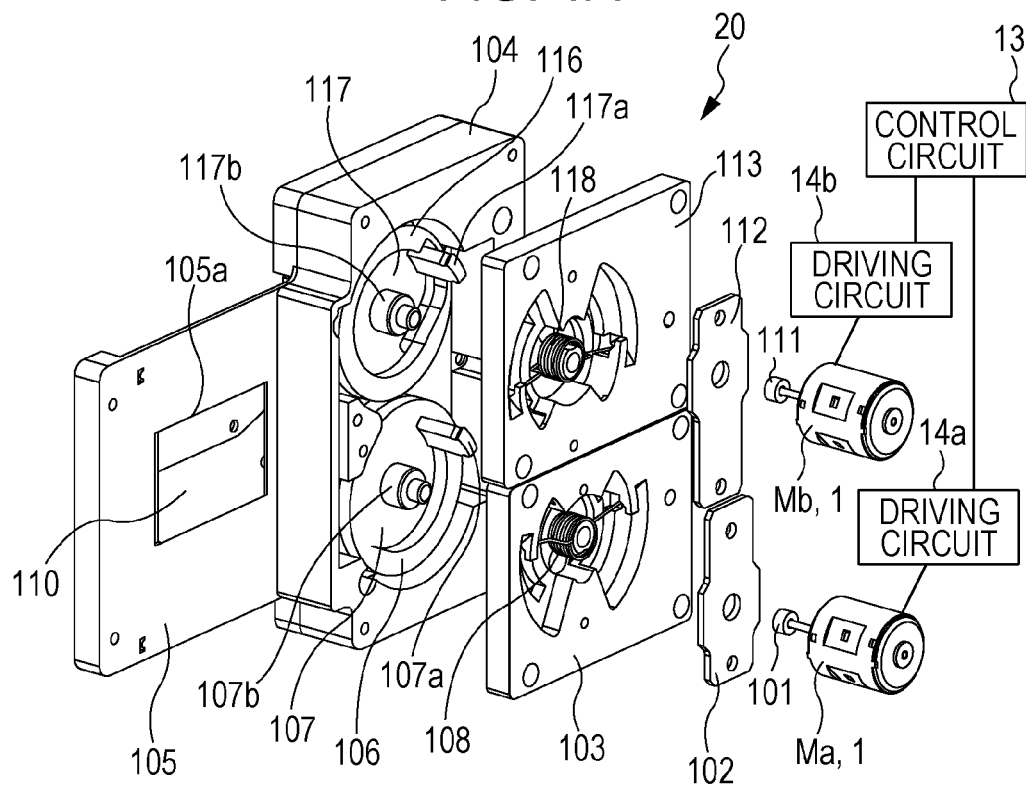


FIG. 1B

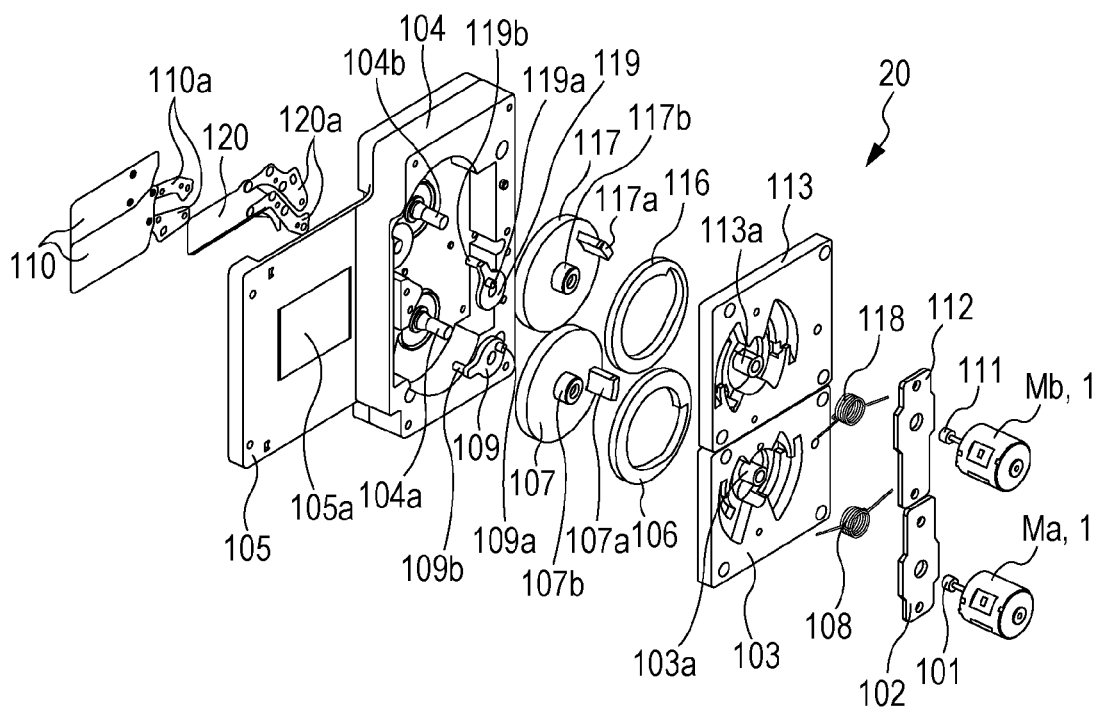


FIG. 2

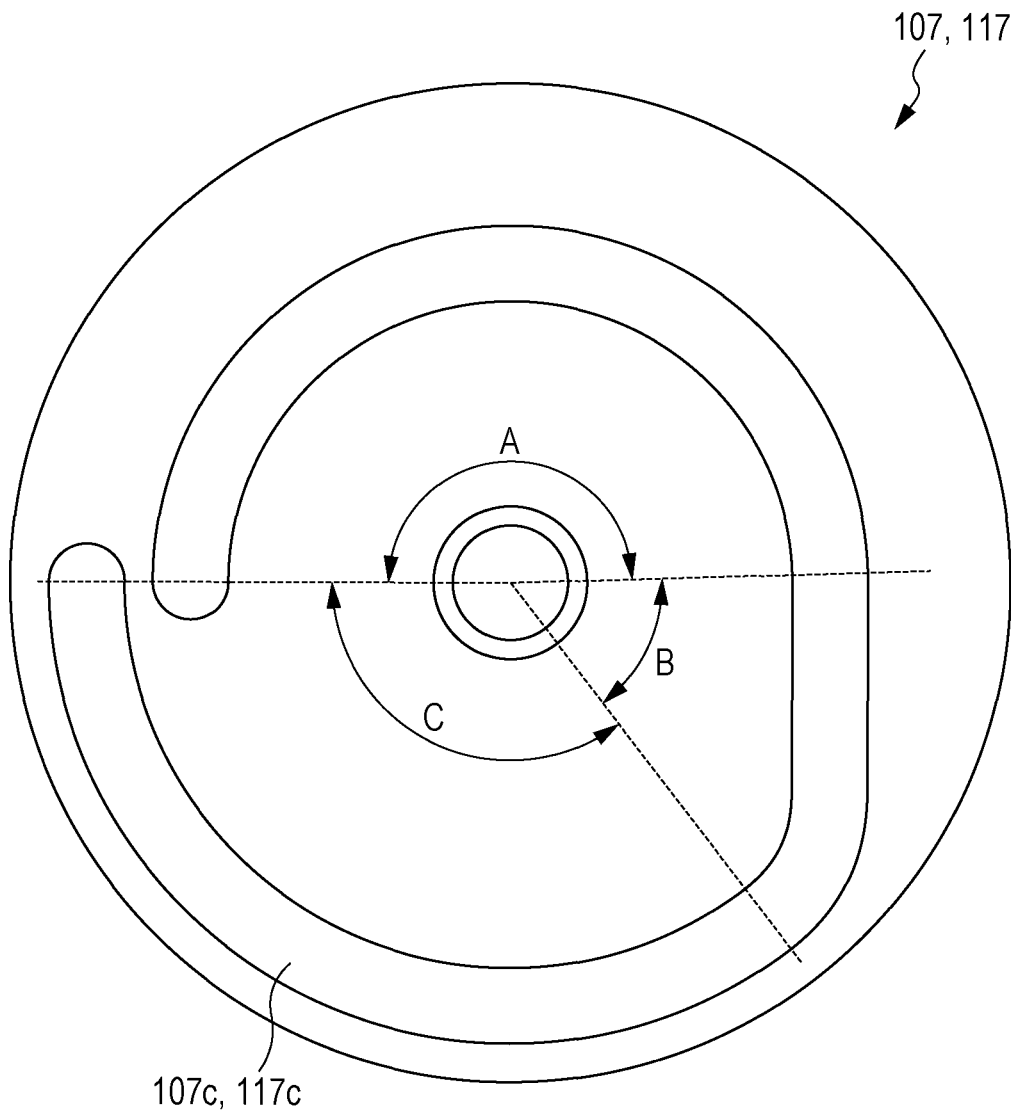


FIG. 3A

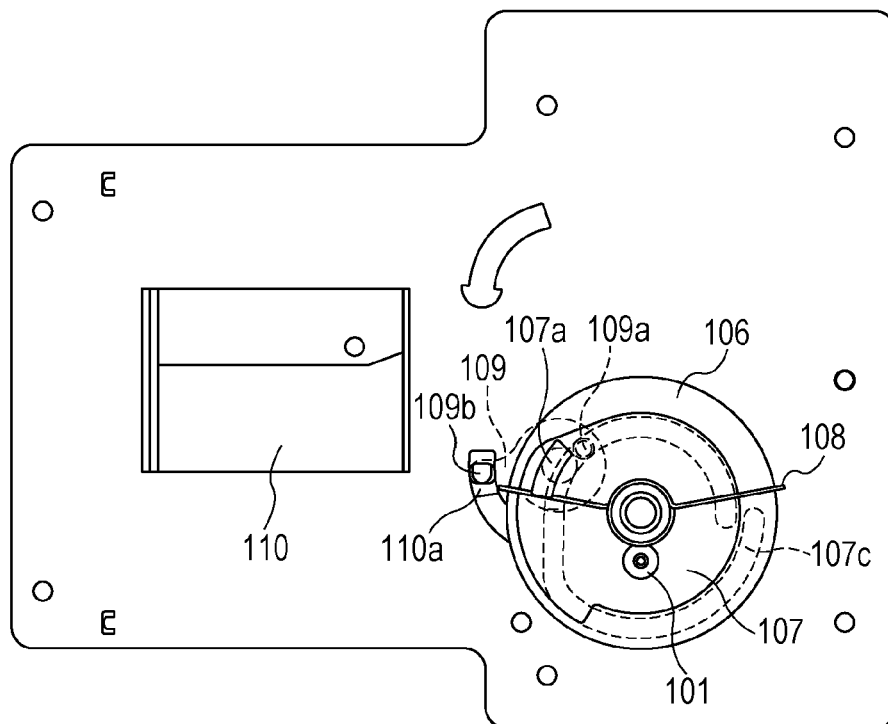


FIG. 3B

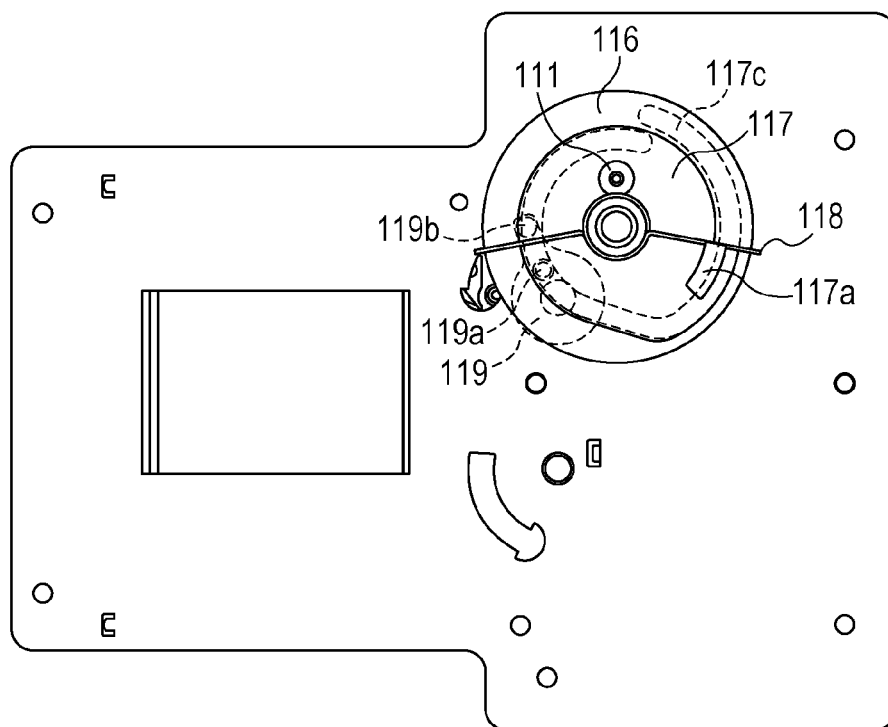


FIG. 4A

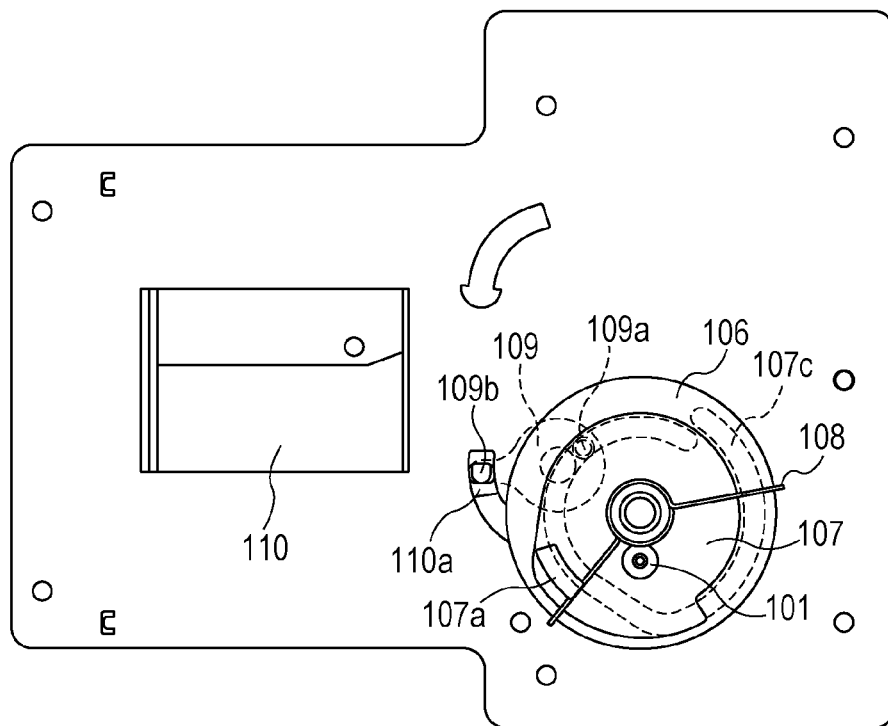


FIG. 4B

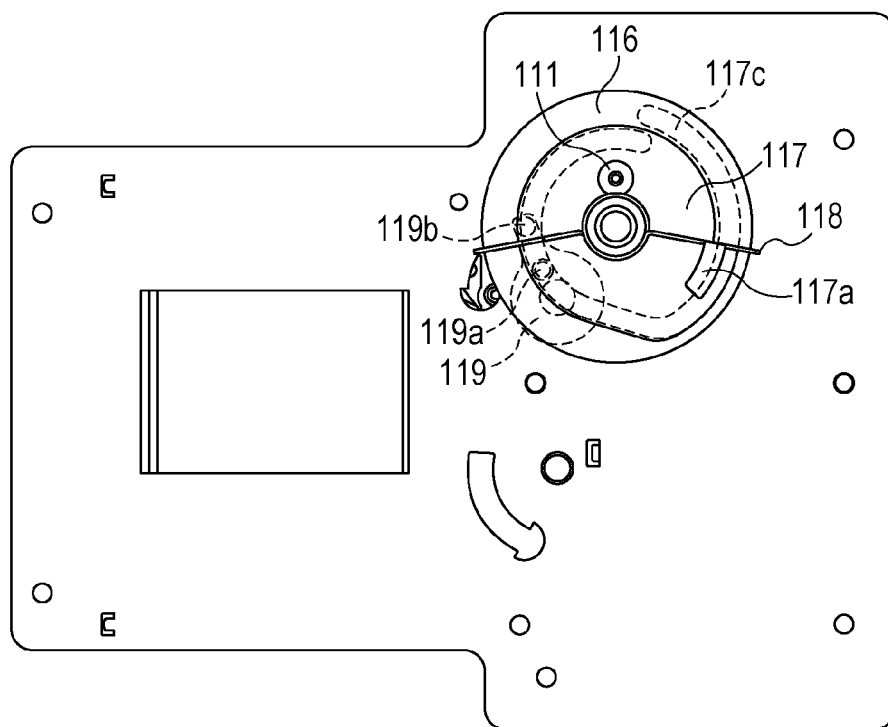


FIG. 5A

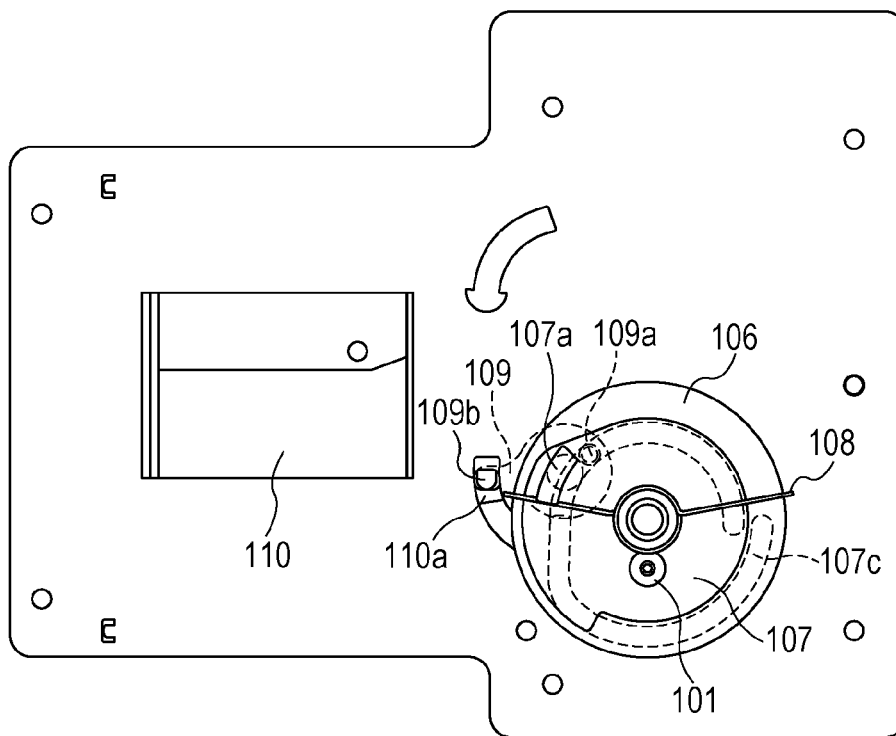


FIG. 5B

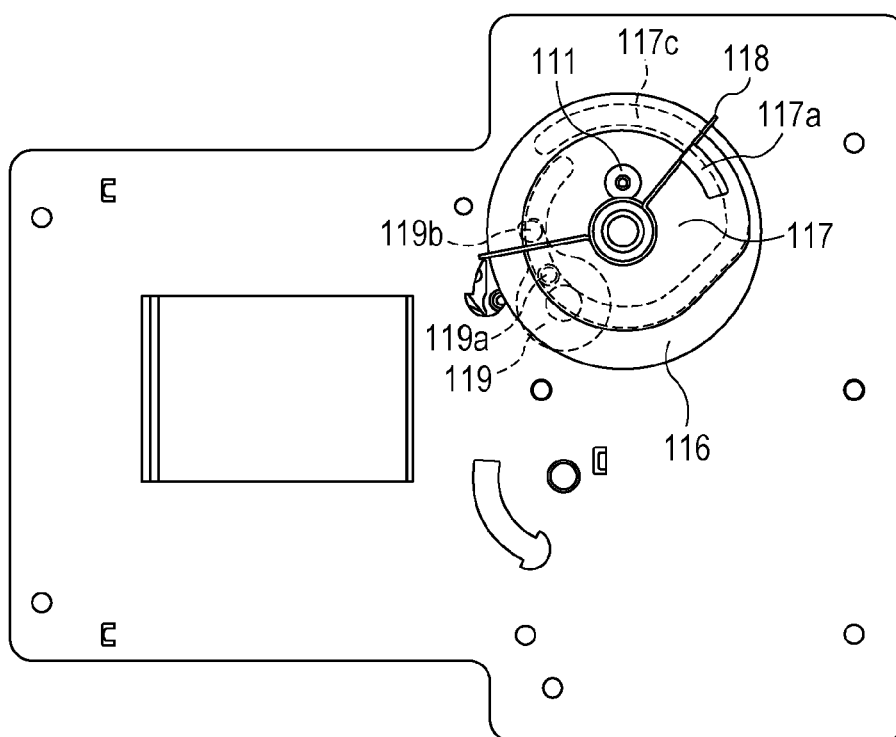


FIG. 6A

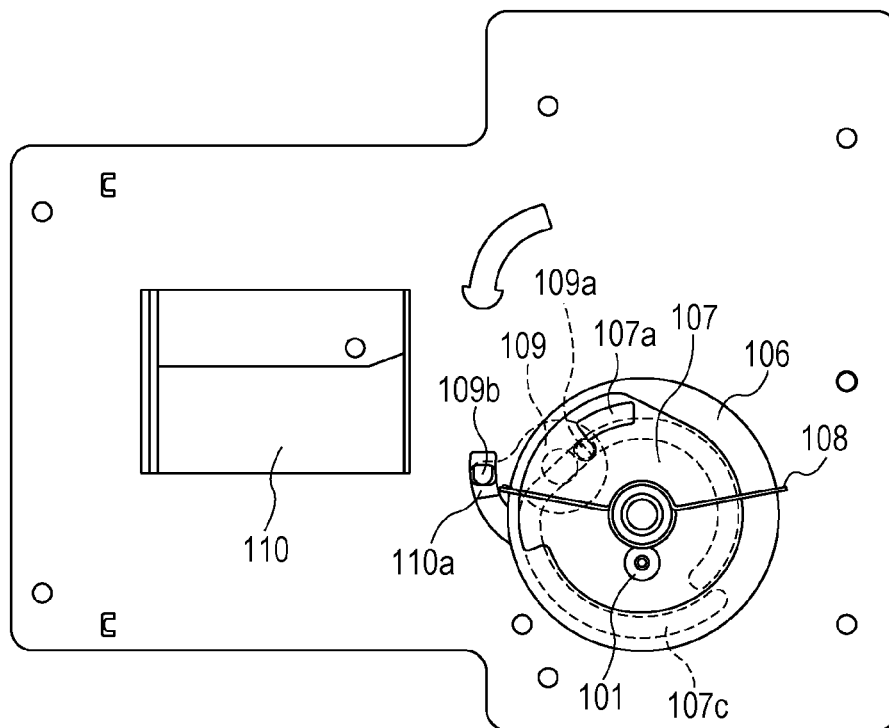


FIG. 6B

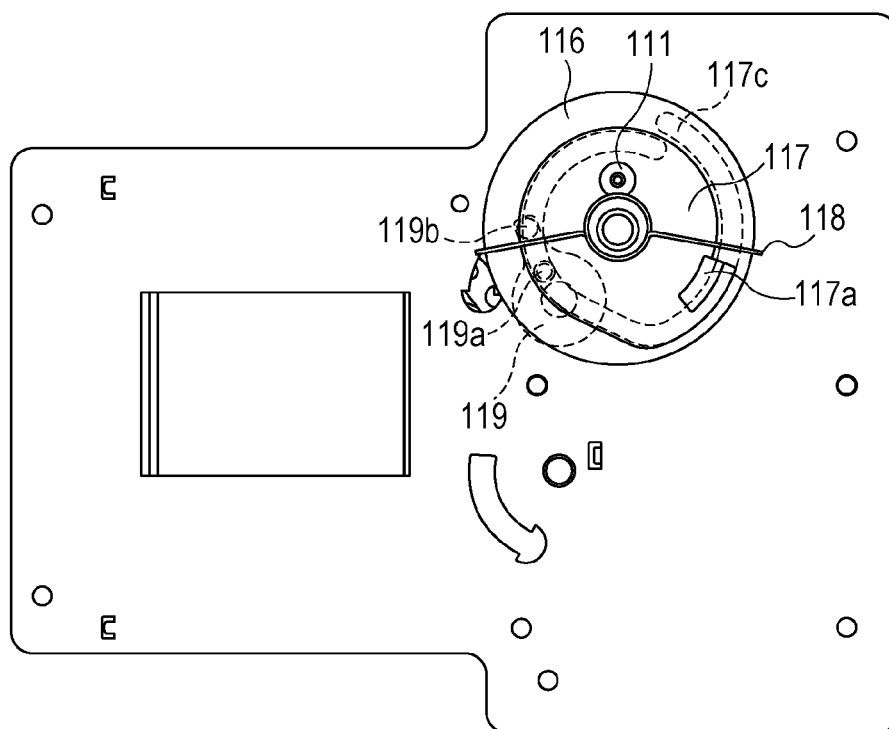


FIG. 7A

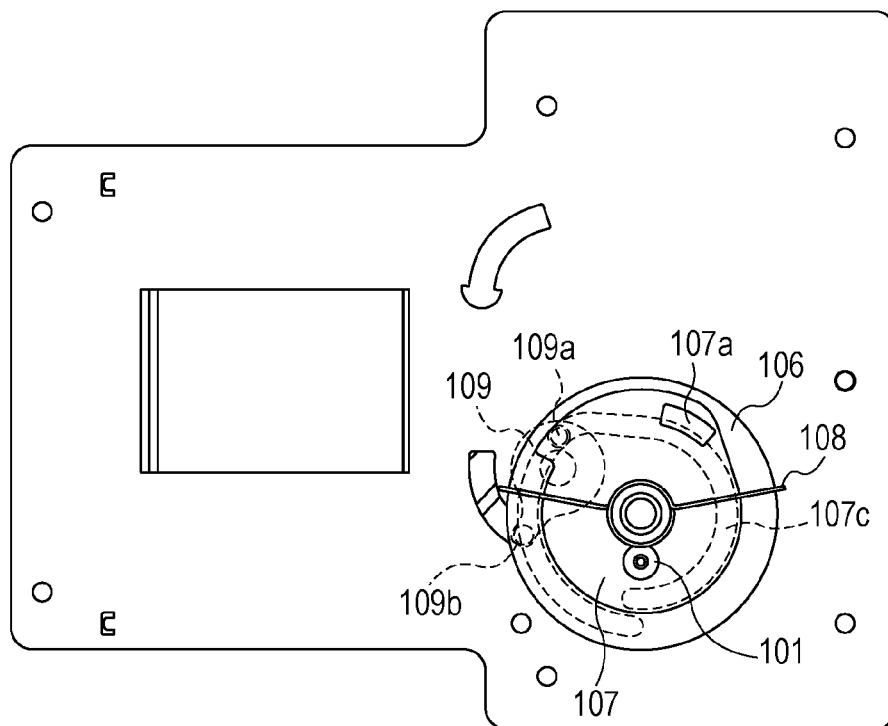


FIG. 7B

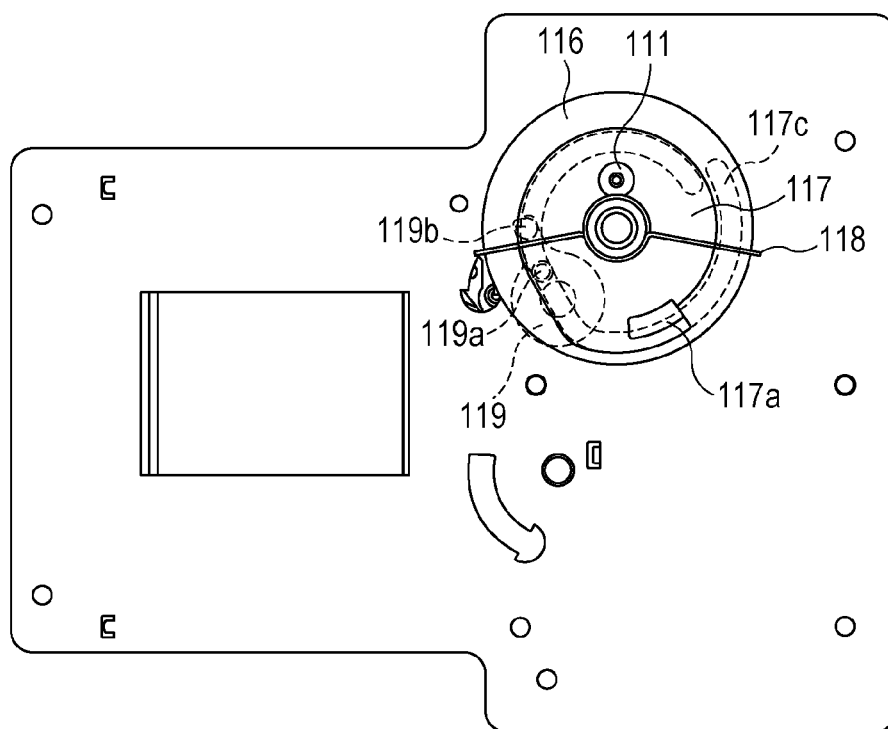


FIG. 8A

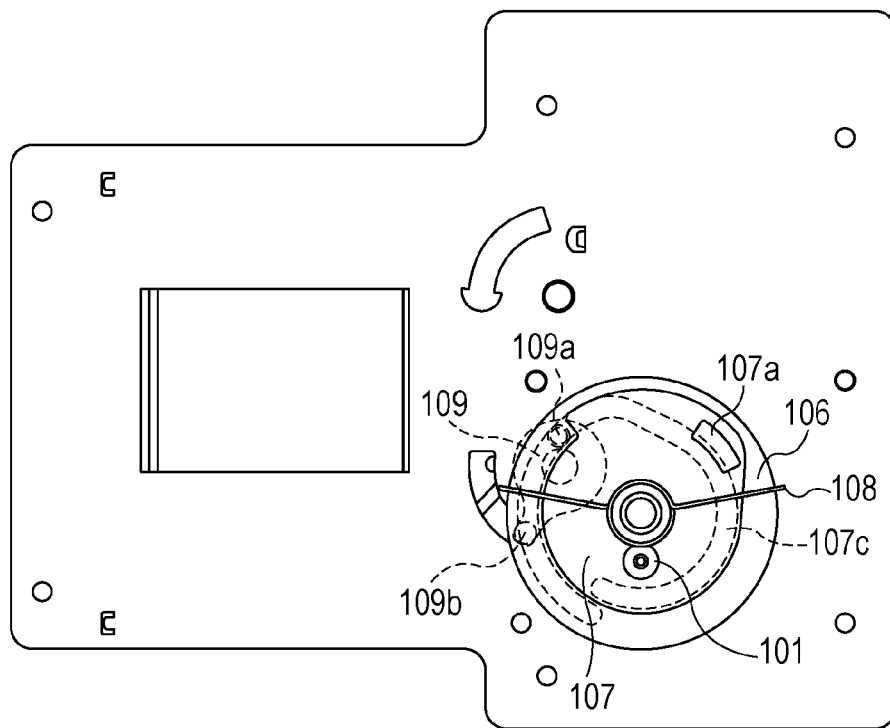


FIG. 8B

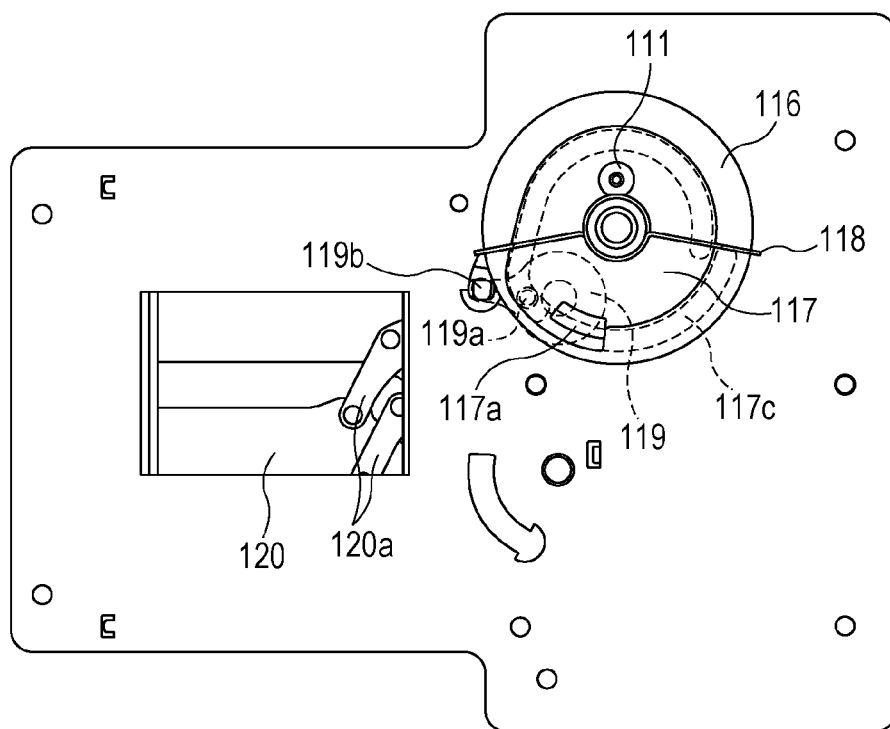


FIG. 9A

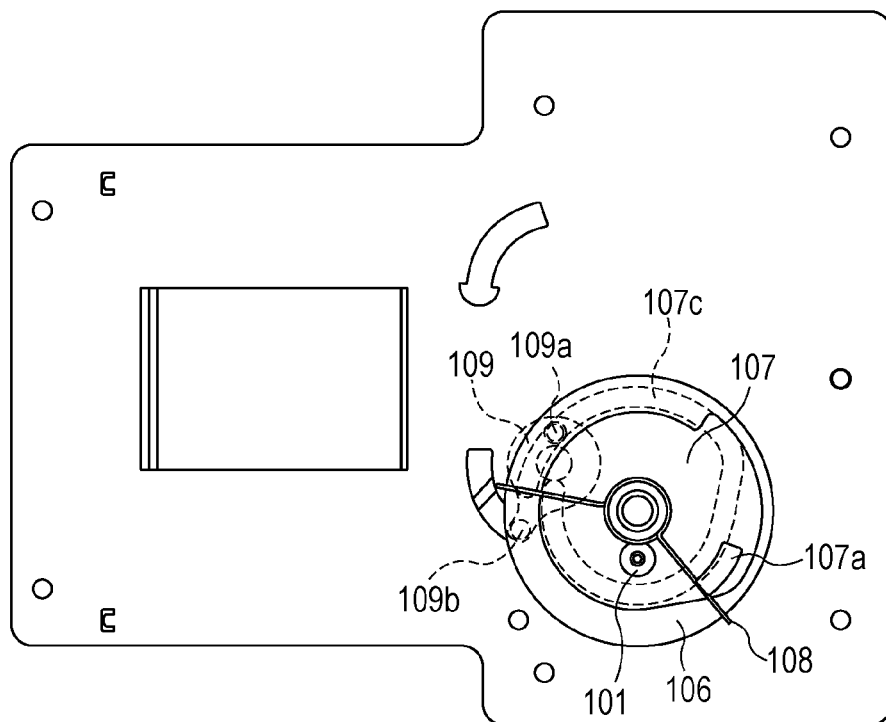


FIG. 9B

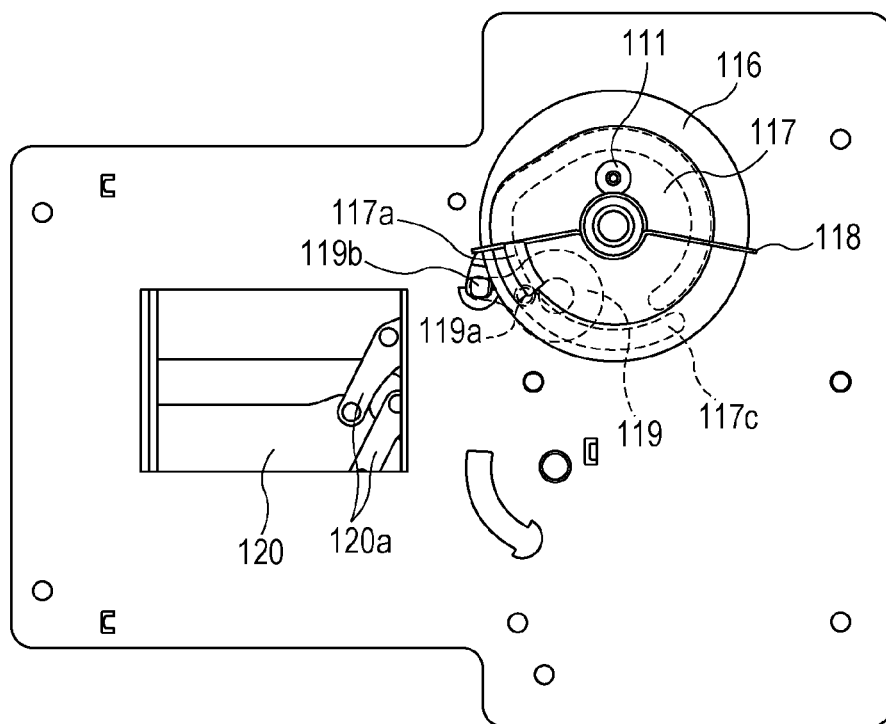


FIG. 10A

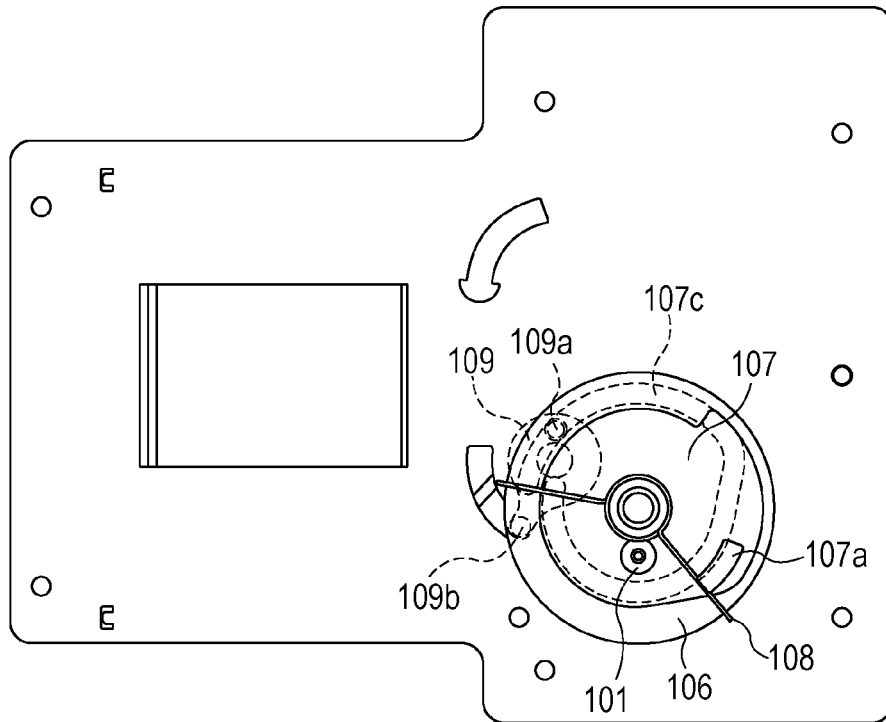


FIG. 10B

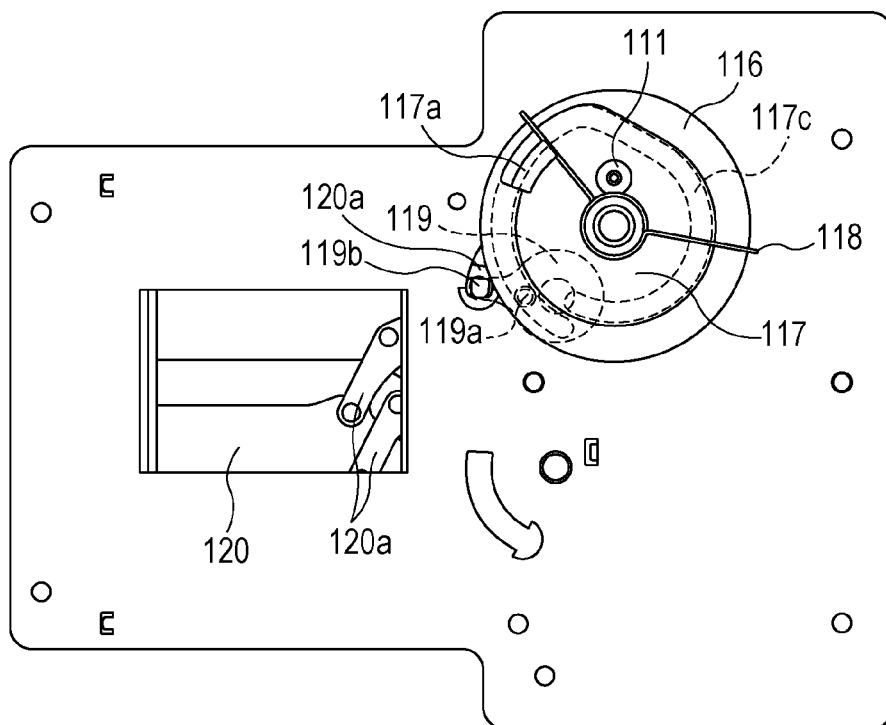


FIG. 11A

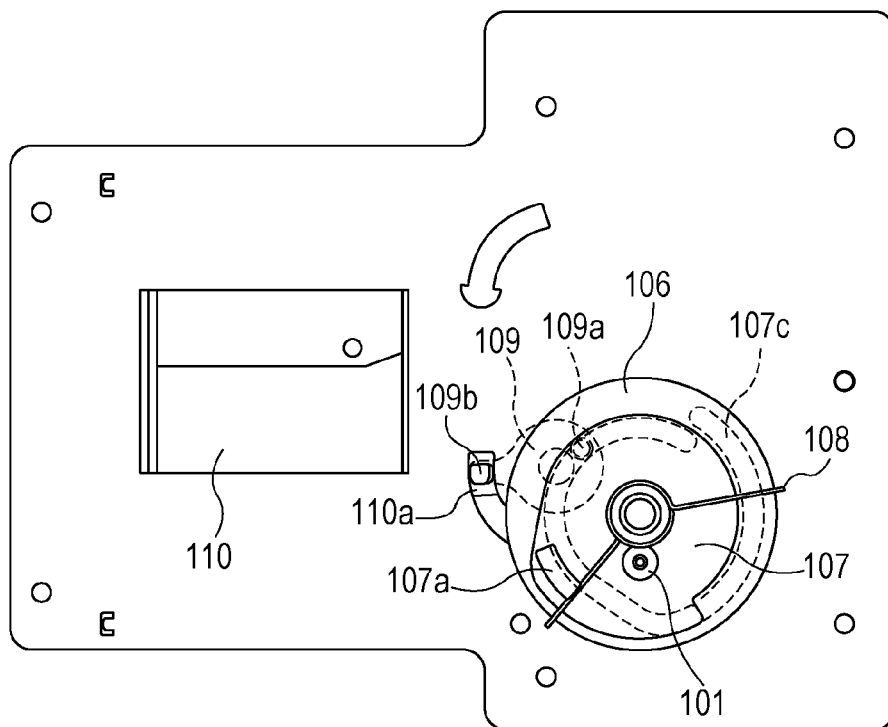


FIG. 11B

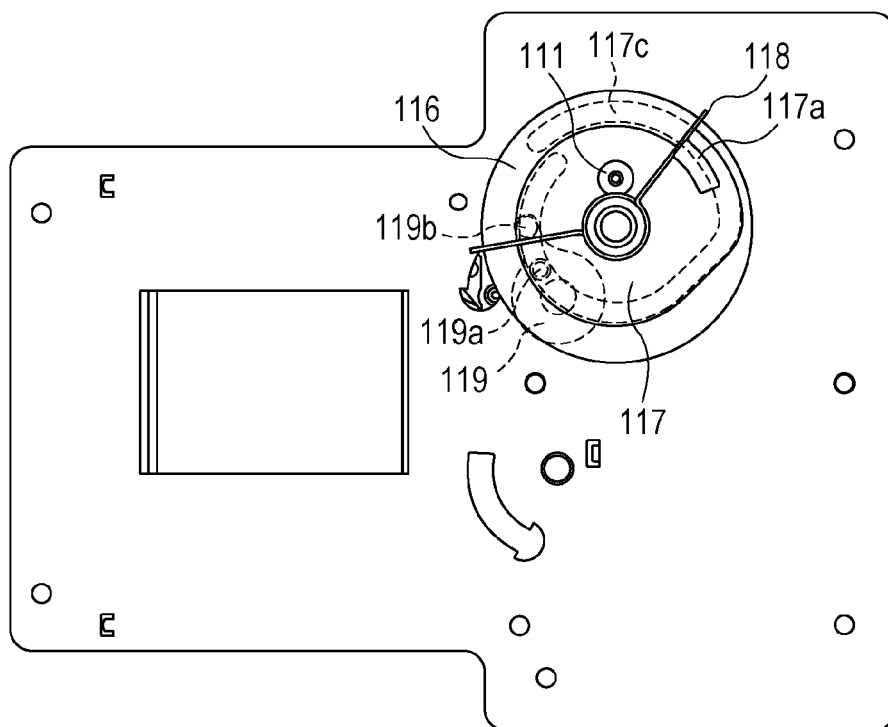


FIG. 12

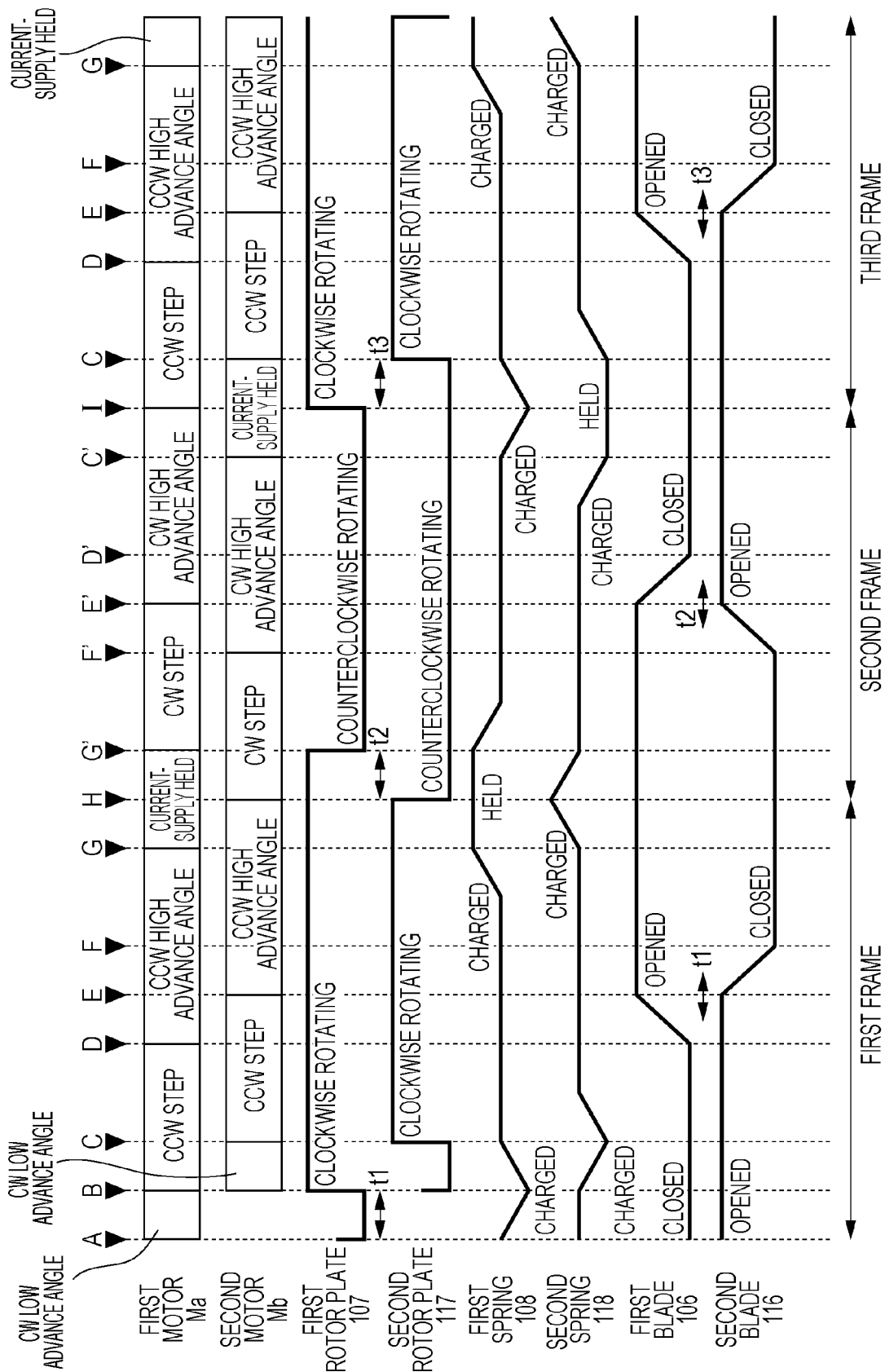


FIG. 13

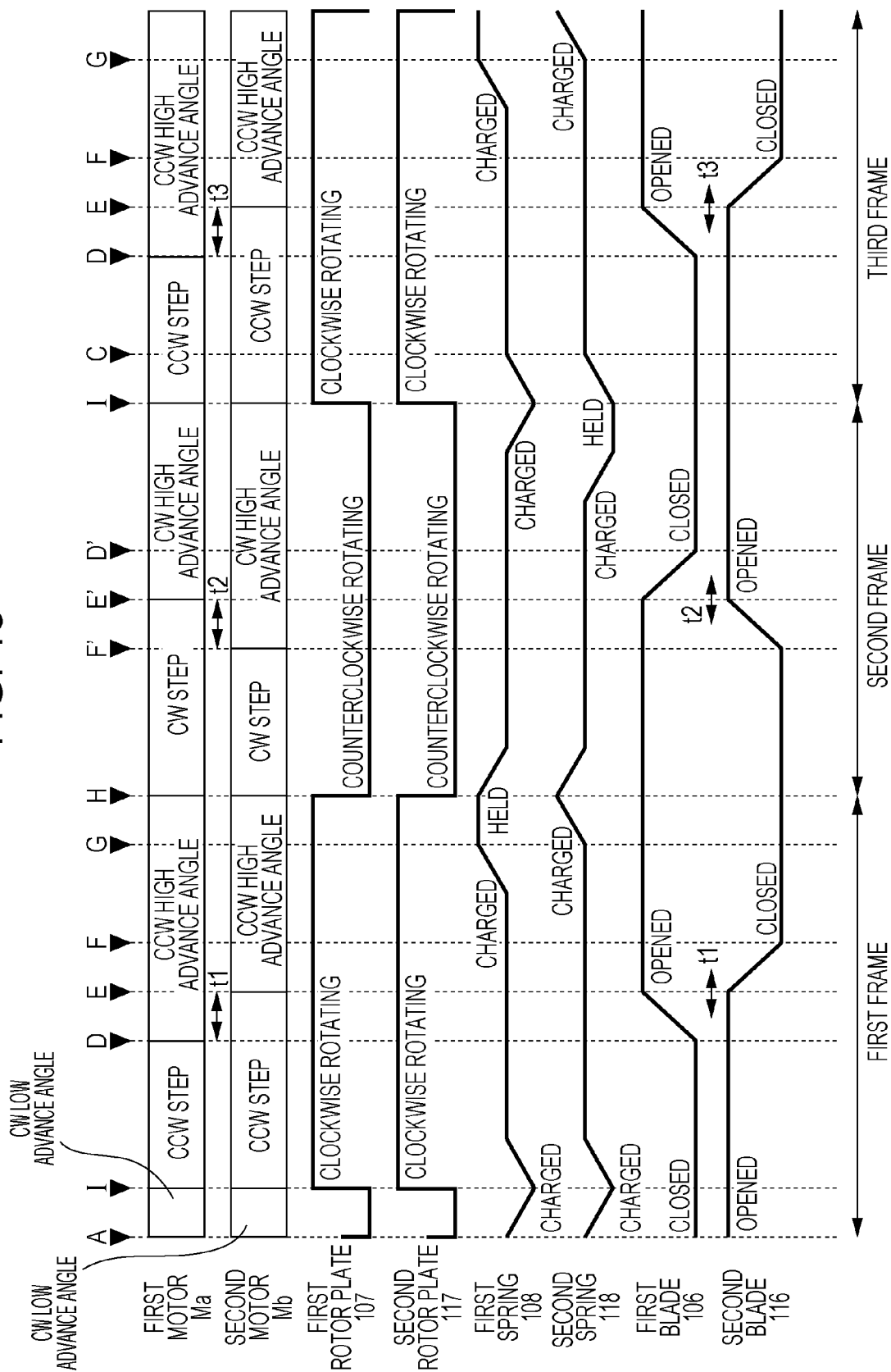


FIG. 14

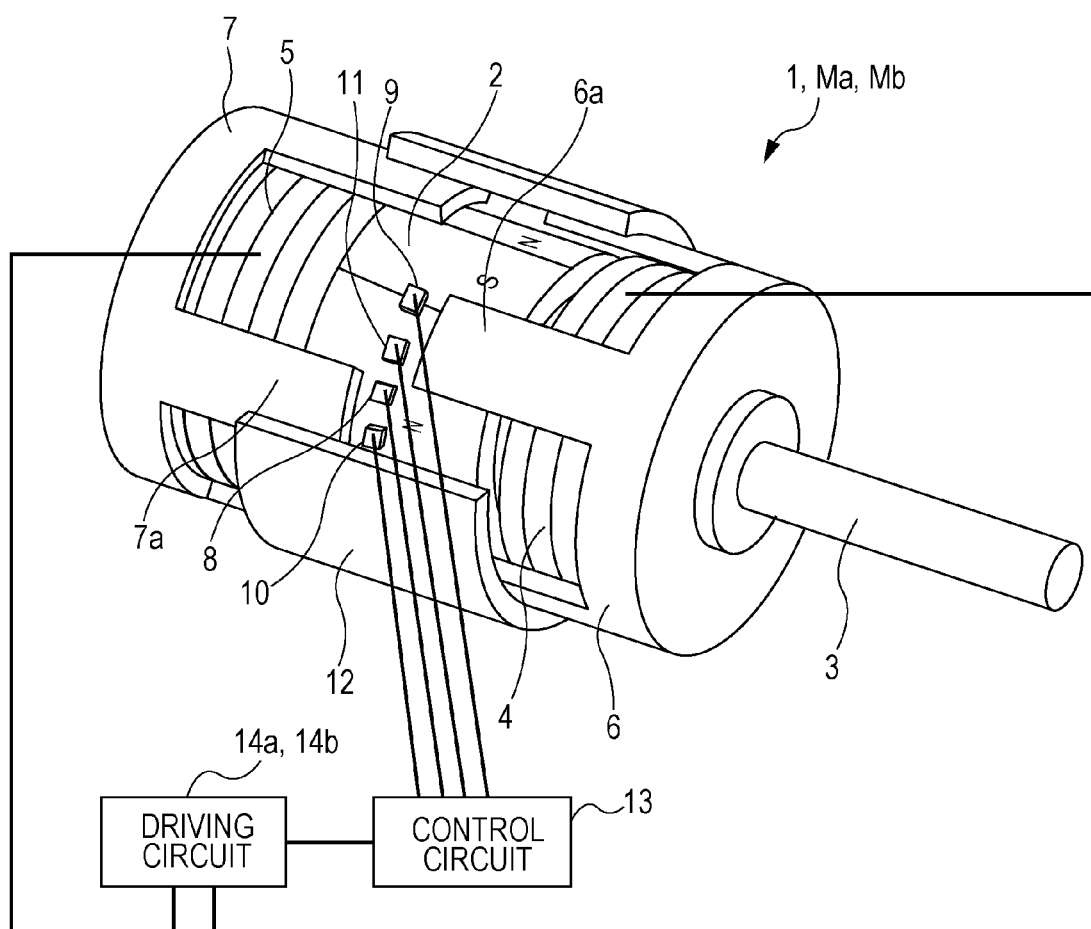


FIG. 15A

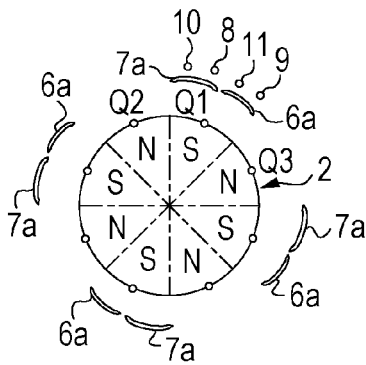


FIG. 15B

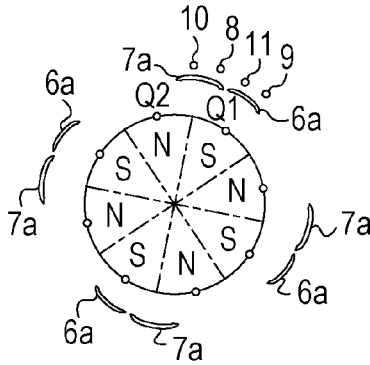


FIG. 15C

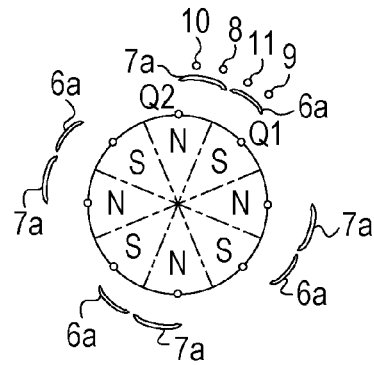


FIG. 15D

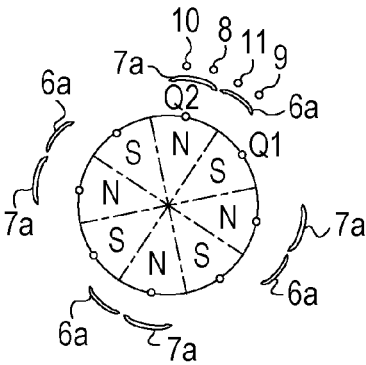


FIG. 15E

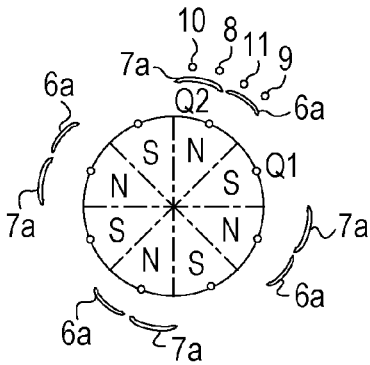


FIG. 15F

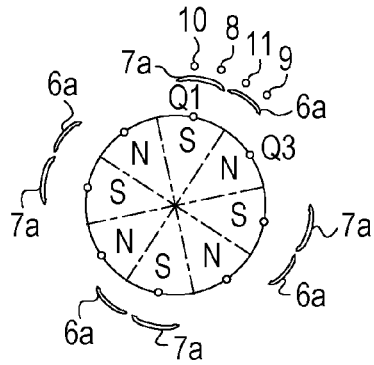


FIG. 15G

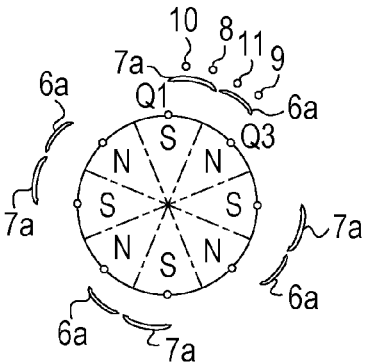


FIG. 15H

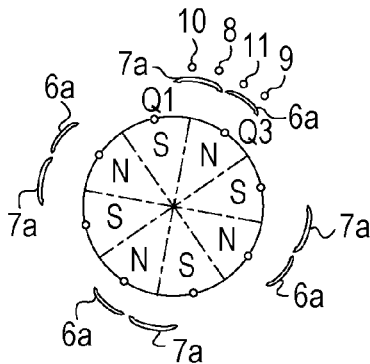


FIG. 15I

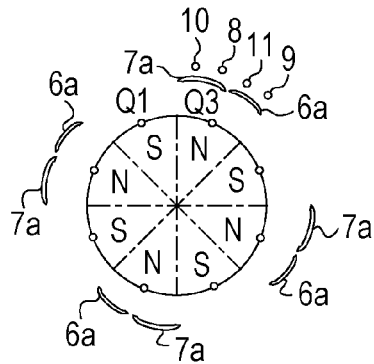


FIG. 16A

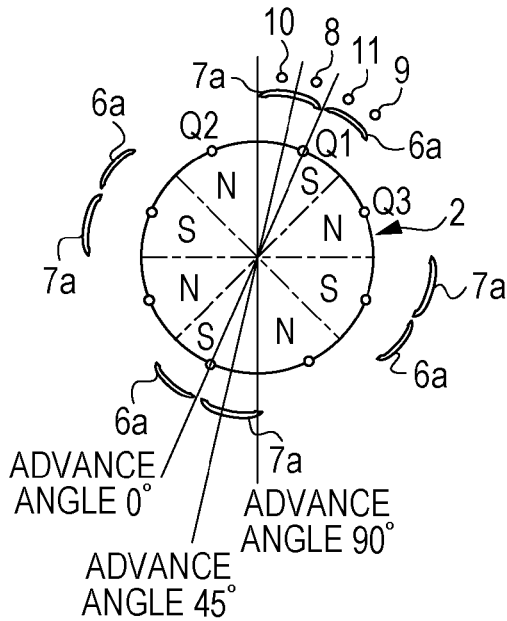


FIG. 16B

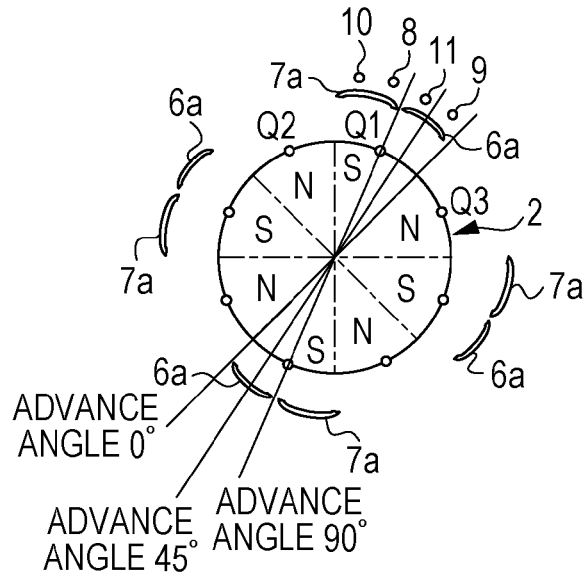


FIG. 16C

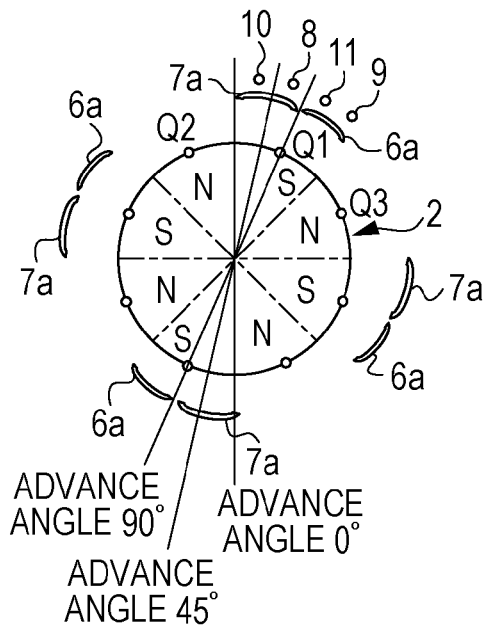
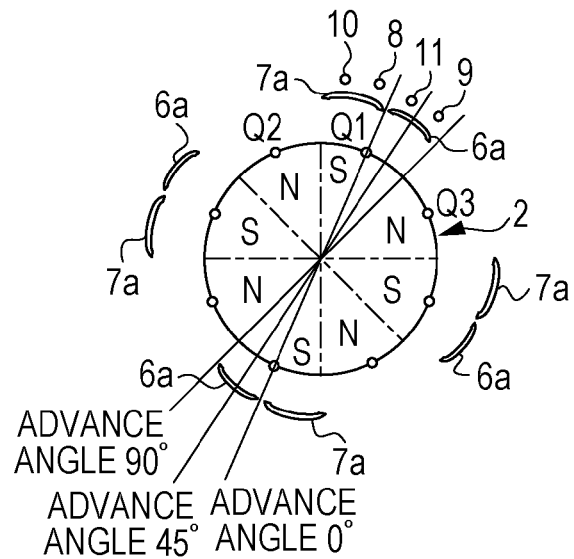
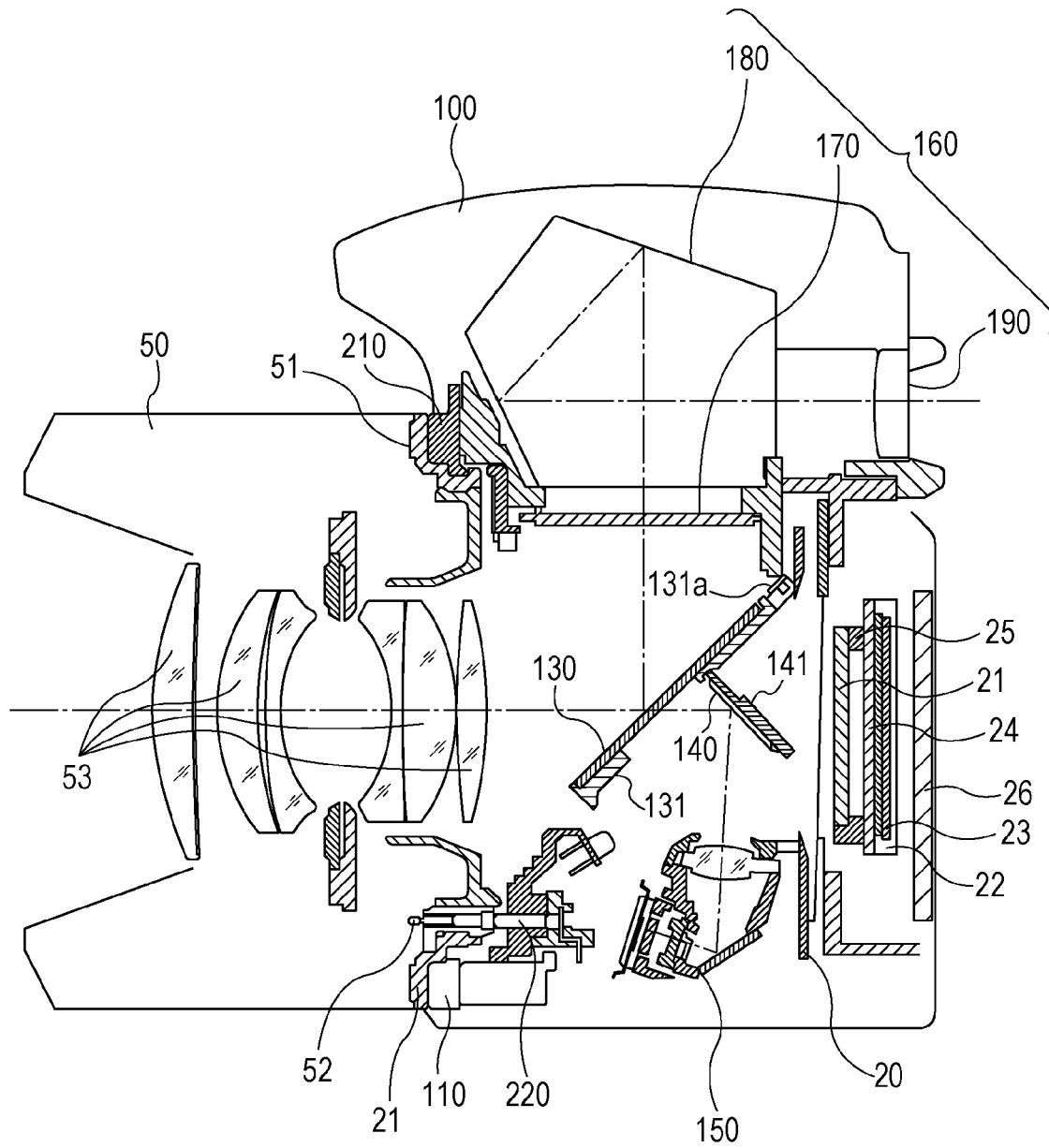


FIG. 16D





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SHUTTER DEVICE AND IMAGE PICKUP APPARATUS INCLUDING SHUTTER DEVICE

TECHNICAL FIELD

The present invention relates to a shutter device and an image pickup apparatus including the shutter device.

BACKGROUND ART

Patent Literature 1 discloses a shutter device in which two shutter blades are made to open or close an opening portion by a stepping motor rotating a driving ring.

The shutter device disclosed in Patent Literature 1 has an acceleration region where the driving ring is rotated, but the two shutter blades do not open or close the opening portion and an exposure region where the two shutter blades are made to open or close the opening portion by rotation of the driving ring. In the shutter device disclosed in Patent Literature 1, after the stepping motor is accelerated in the acceleration region, the two shutter blades open or close the opening portion in the exposure region.

CITATION LIST

Patent Literature

PTL 1 Japanese Patent Laid-Open No. 7-56211

For the shutter device disclosed in Patent Literature 1, in the exposure region, a load for moving the two shutter blades may cause the stepping motor to lose synchronization.

That is, when the stepping motor is used as a driving source for the stepping motor, if the stepping motor loses synchronization because of variations in load during driving, it becomes unable to rotate the driving ring at that time, and this disables an exposure operation.

It is an object of the present invention to provide a shutter device in which, when a stepping motor drives a driven member and thus a light blocking member moves from a closed state to an open state or from the open state to the closed state, the stepping motor does not lose synchronization.

SUMMARY OF INVENTION

A shutter device according to an aspect of the present invention includes a stepping motor, a driven member, and a light shielding member. The stepping motor is configured to be driven in open-loop driving mode at which an energization state of a coil is switched at predetermined time intervals and in feed-back driving mode at which the energization state of the coil is switched in accordance with a rotation position of a rotor. The driven member is configured to be driven by the stepping motor. The light shielding member is configured to move to a closed state in which an aperture is closed and to an open state in which the aperture is open in coordination with driving the driven member. The driven member is configured to be driven in a first zone where the driven member is driven by the stepping motor, but the light shielding member remains in the closed state or the open state and in a second zone where the driven member is driven by the stepping motor, and thus the light shielding member moves from the closed state to the open state or from the open state to the closed state. The driven member is driven in the first zone by the stepping motor in one direction, and after the driven member is driven in the first zone, the driven member is driven in the second zone. In a case where the driven member is driven in the first zone, the stepping motor drives the driven member in the

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open-loop driving mode. In a case where the driven member is driven in the second zone, the stepping motor drives the driven member in the feed-back driving mode.

Further features of the present invention will become apparent from the following description of exemplary embodiments with reference to the attached drawings.

BRIEF DESCRIPTION OF DRAWINGS

FIGS. 1A and 1B are illustrations for describing a shutter unit 20 as a shutter according to one embodiment of the present invention.

FIG. 2 is an illustration of a first rotor plate 107 (second rotor plate 117) as seen from a back surface side.

FIGS. 3A and 3B are illustrations for describing a state of the shutter unit 20 in A status.

FIGS. 4A and 4B are illustrations for describing a state of the shutter unit 20 in B status.

FIGS. 5A and 5B are illustrations for describing a state of the shutter unit 20 in C status.

FIGS. 6A and 6B are illustrations for describing a state of the shutter unit 20 in D status.

FIGS. 7A and 7B are illustrations for describing a state of the shutter unit 20 in E status.

FIGS. 8A and 8B are illustrations for describing a state of the shutter unit 20 in F status.

FIGS. 9A and 9B are illustrations for describing a state of the shutter unit 20 in G status.

FIGS. 10A and 10B are illustrations for describing a state of the shutter unit 20 in H status.

FIGS. 11A and 11B are illustrations for describing a state of the shutter unit 20 in I status.

FIG. 12 is a timing chart for describing operations of the shutter unit 20 when a camera 100 is operating in continuous shooting mode.

FIG. 13 is a timing chart for describing operations of the shutter unit 20 when the camera 100 is operating in continuous shooting mode as a variation of the embodiment.

FIG. 14 illustrates a motor 1 used as each of a first motor Ma and a second motor Mb.

FIGS. 15A to 15I are illustrations for describing operations of the motor.

FIGS. 16A to 16D are illustrations for describing positions in which a first magnetic sensor 8, a second magnetic sensor 9, a third magnetic sensor 10, and a fourth magnetic sensor 11 are arranged.

FIG. 17 is a central sectional view of the digital single-lens reflex camera body 100 as an image pickup apparatus according to one embodiment of the present invention and an interchangeable lens 50.

DESCRIPTION OF EMBODIMENTS

Embodiments of the present invention are described in detail below with reference to the drawings.

FIG. 17 is a central sectional view of a digital single-lens reflex camera body (hereinafter referred to as camera) 100 according to one embodiment of the present invention and an interchangeable lens 50 as an image pickup apparatus.

The interchangeable lens 50 is detachably fixed on the camera 100 with a mount section 210 in the camera 100 and a mount section 51 in the interchangeable lens 50. When the interchangeable lens 50 is attached to the camera 100, a contact section 220 in the camera 100 and a contact section 52 in the interchangeable lens 50 are electrically connected to each other.

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A light flux that has passed through focus lenses **53** in the interchangeable lens **50** enters a main mirror **130** in the camera **100**. The main mirror **130** is held on a main mirror holding frame **131** and is supported by a rotating shaft section **131a** so as to be able to pivot between a mirror upper position and a mirror lower position.

The main mirror **130** is a semitransparent mirror. A light flux that has passed through the main mirror **130** is reflected downward by a sub mirror **140** and is guided to a focus detecting unit **150**.

The sub mirror **140** is held on a sub mirror holding frame **141**. The sub mirror holding frame **141** is supported by a hinge shaft (not illustrated) so as to be able to pivot with respect to the main mirror holding frame **131**.

The focus detecting unit **150** is configured to detect the amount of defocusing of the focus lenses **53** and calculate the amount of driving of the focus lenses **53** for achieving focus for the focus lenses **53**. The interchangeable lens **50** is configured to receive the calculated amount of driving through the contact sections **220** and **52**. The interchangeable lens **50** is configured to adjust the focus by controlling a motor (not illustrated) and driving the focus lenses **53** on the basis of the received amount of driving.

A light flux reflected by the main mirror **130** is guided to an optical viewfinder **160**. The optical viewfinder **160** includes a focusing plate **170**, a pentaprism **180**, and an eyepiece **190**. The light flux guided to the optical viewfinder **160** forms an object image on the focusing plate **170**. A user can observe the object image on the focusing plate **170** through the pentaprism **180** and the eyepiece **190**.

A shutter unit **20** is arranged behind the sub mirror **140**. An optical low-pass filter **21**, an image pickup element holder **22**, an image pickup element **23**, a cover member **24**, and a rubber member **25** are arranged behind the shutter unit **20**. In shooting, a light flux that has passed through the optical low-pass filter **21** enters the image pickup element **23**. The image pickup element holder **22** is fixed to the housing of the camera **100** with a screw (not illustrated). The image pickup element **23** is held by the image pickup element holder **22**. The cover member **24** protects the image pickup element **23**. The rubber member **25** holds the optical low-pass filter **21** and hermetically seals the gap between the optical low-pass filter **21** and the image pickup element **23**.

A display monitor **26** may be a liquid crystal display monitor and is configured to display a shot image and display various setting statuses of the camera **100**.

FIGS. **1A** and **1B** are illustrations for describing the shutter unit **20** as a shutter according to one embodiment of the present invention. FIG. **1A** is an exploded perspective view for describing a configuration of the shutter unit **20**. FIG. **1B** is an exploded perspective view illustrating the shutter unit **20** further disassembled from the state illustrated in FIG. **1A**.

As illustrated in FIG. **1A**, the shutter unit **20** is driven by a first motor **Ma** and a second motor **Mb**. The first motor **Ma** is connected to a driving circuit **14a**. The second motor **Mb** is connected to a driving circuit **14b**. The driving circuit **14a** and the driving circuit **14b** are connected to a control circuit **13**. In the present embodiment, the first motor **Ma** and the second motor **Mb** are the same motors. A pinion gear **101** is press-fit to the output shaft of the first motor **Ma**. A pinion gear **111** is press-fit to the output shaft of the second motor **Mb**.

The first motor **Ma** is mounted to a motor mounting plate **102**. The motor mounting plate **102** is fixed to a cover plate **103**. The second motor **Mb** is mounted to a motor mounting plate **112**. The motor mounting plate **112** is fixed to a cover plate **113**.

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A driving mechanism accommodating section **104** accommodates a first rotor plate **107** to which a weight **106** is bonded and a second rotor plate **117** to which a weight **116** is bonded. The first rotor plate **107** includes a protruding section **107a**. When the cover plate **103** is mounted on the driving mechanism accommodating section **104**, the protruding section **107a** is exposed through the cover plate **103**. The second rotor plate **117** includes a protruding section **117a**. When the cover plate **113** is mounted on the driving mechanism accommodating section **104**, the protruding section **117a** is exposed through the cover plate **113**. A first spring **108** is mounted to the cover plate **103**. A second spring **118** is mounted to the cover plate **113**.

The first rotor plate **107** includes a gear section **107b**. When the motor mounting plate **102** is fixed on the cover plate **103**, the pinion gear **101** and the gear section **107b** engage with each other. The second rotor plate **117** includes a gear section **117b**. When the motor mounting plate **112** is fixed on the cover plate **113**, the pinion gear **111** and the gear section **117b** engage each other.

Accordingly, when the first motor **Ma** is driven, the first rotor plate **107** rotates; when the second motor **Mb** is driven, the second rotor plate **117** rotates.

A blade accommodating section **105** has an aperture **105a**. The blade accommodating section **105** accommodates a first blade **110** and a second blade **120**.

As illustrated in FIG. **1B**, a driving arm **110a** is mounted to the first blade **110**. A driving arm **120a** is mounted to the second blade **120**.

A first driving lever **109** and a second driving lever **119** are supported on the driving mechanism accommodating section **104**. The first driving lever **109** includes a cam pin **109a** and an engagement pin **109b**. The cam pin **109a** engages with a cam groove **107c** in the first rotor plate **107**. The engagement pin **109b** engages with the driving arm **110a**. When the first driving lever **109** pivots, the first blade **110** opens or closes the aperture **105a**. Similarly, the second driving lever **119** includes a cam pin **119a** and an engagement pin **119b**. The cam pin **119a** engages with a cam groove **117c** in the second rotor plate **117**. The engagement pin **119b** engages with the driving arm **120a**. When the second driving lever **119** pivots, the second blade **120** opens or closes the aperture **105a**. In the present embodiment, the first driving lever **109** and the second driving lever **119** are the same components.

The driving mechanism accommodating section **104** includes a shaft section **104a** and a shaft section **104b**. The first rotor plate **107** is supported by the shaft section **104a**. The second rotor plate **117** is supported by the shaft section **104b**. The first rotor plate **107** includes the gear section **107b** on its front surface. The weight **106** is bonded and fixed to the circumferential section of the first rotor plate **107**. The first rotor plate **107** includes the cam groove **107c**, with which the cam pin **109a** engages, in its back surface.

Similarly, the second rotor plate **117** includes the gear section **117b** on its front surface. The weight **116** is bonded and fixed to the circumferential section of the second rotor plate **117**. The second rotor plate **117** includes the cam groove **117c**, with which the cam pin **119a** engages, in its back surface. In the present embodiment, the first rotor plate **107** and the second rotor plate **117** are the same components. The weight **106** and the weight **116** are the same components.

Each of the first rotor plate **107** and the second rotor plate **117** functions as a driven member. The first blade **110** and the first driving lever **109** function as a light shielding member capable of moving between a closed state where they closes the aperture **105a** and an open state where they opens the aperture **105a** in coordination with driving the first rotor plate

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107. The second blade 120 and the second driving lever 119 function as a light shielding member capable of moving between a closed state where they closes the aperture 105a and an open state where they opens the aperture 105a in coordination with driving the second rotor plate 117. Each of the first spring 108 and the second spring 118 functions as an urging member.

FIG. 2 is an illustration of the first rotor plate 107 (second rotor plate 117) as seen from the back surface side. The cam groove 107c (cam groove 117c), with which the cam pin 109a (cam pin 119a) engages, are disposed in the back surface of the first rotor plate 107 (second rotor plate 117). As illustrated in FIG. 2, a first idle running driving region A, an exposure driving region B, and a second idle running driving region C are set in the cam groove 107c (cam groove 117c). In the first idle running driving region A and the second idle running driving region C in the cam groove 107c (cam groove 117c), the cam lift is substantially zero.

When the cam pin 109a (cam pin 119a) follows the first idle running driving region A or the second idle running driving region C, the first driving lever 109 (second driving lever 119) does not rotate and the first blade 110 (second blade 120) remains in a closed state or an open state.

When the cam pin 109a (cam pin 119a) follows the exposure driving region B, the first driving lever 109 (second driving lever 119) rotates and the first blade 110 (second blade 120) moves from the closed state to the open state or from the open state to the closed state.

When the first rotor plate 107 (second rotor plate 117) rotates clockwise, the cam pin 109a (cam pin 119a) follows the first idle running driving region A, the exposure driving region B, and the second idle running driving region C in this order.

The details of the clockwise rotation of the first rotor plate 107 (second rotor plate 117) are described below.

The first idle running driving region A is a first cam region. The zone where the cam pin 109a (cam pin 119a) follows the first idle running driving region A is a first zone.

The exposure driving region B is a second cam region. The zone where the cam pin 109a (cam pin 119a) follows the exposure driving region B is a second zone.

The second idle running driving region C is a third cam region. The zone where the cam pin 109a (cam pin 119a) follows the second idle running driving region C is a third zone.

In contrast, when the first rotor plate 107 (second rotor plate 117) rotates counterclockwise, the cam pin 109a (cam pin 119a) follows the second idle running driving region C, the exposure driving region B, and the first idle running driving region A in this order.

The details of the counterclockwise rotation of the first rotor plate 107 (second rotor plate 117) are described below.

The second idle running driving region C is the first cam region. The zone where the cam pin 109a (cam pin 119a) follows the second idle running driving region C is the first zone.

The exposure driving region B is the second cam region. The zone where the cam pin 109a (cam pin 119a) follows the exposure driving region B is the second zone.

The first idle running driving region A is the third cam region. The zone where the cam pin 109a (cam pin 119a) follows the first idle running driving region A is the third zone.

That is, the first rotor plate 107 (second rotor plate 117) is driven in one direction, and thus the first rotor plate 107 (second rotor plate 117) is driven in the first zone. After the

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first rotor plate 107 (second rotor plate 117) is driven in the first zone, the first rotor plate 107 (second rotor plate 117) is driven in the second zone.

As illustrated in FIG. 1B, the cover plate 103 is provided with a hollow shaft section 103a. When the cover plate 103 is mounted on the driving mechanism accommodating section 104, the protruding section 107a in the first rotor plate 107 is exposed through the cover plate 103 and the shaft section 104a is fit into an inner section of the hollow shaft section 103a. The first spring 108 is mounted on an outer section of the hollow shaft section 103a.

Similarly, the cover plate 113 is provided with a hollow shaft section 113a. When the cover plate 113 is mounted on the driving mechanism accommodating section 104, the protruding section 117a in the second rotor plate 117 is exposed through the cover plate 113 and the shaft section 104b is fit into an inner section of the hollow shaft section 113a. The second spring 118 is mounted on an outer section of the hollow shaft section 113a.

When the motor mounting plate 102 with the first motor Ma mounted thereon is mounted on the cover plate 103, the output shaft of the first motor Ma penetrates through an opening in the cover plate 103, and the pinion gear 101 and the gear section 107b engage with each other. Similarly, when the motor mounting plate 112 with the second motor Mb mounted thereon is mounted on the cover plate 113, the output shaft of the second motor Mb penetrates through an opening in cover plate 113, and the pinion gear 111 and the gear section 117b engage with each other.

In the present embodiment, the first motor Ma, the first rotor plate 107, the first spring 108, the first driving lever 109, and the first blade 110 constitute a first shutter driving mechanism. The second motor Mb, the second rotor plate 117, the second spring 118, the second driving lever 119, and the second blade 120 constitute a second shutter driving mechanism.

Each of the first motor Ma and the second motor Mb is a stepping motor that can be driven in step-driving (open-loop driving) at which an energization state of the coil is switched at predetermined time intervals and in two types of feed-back driving with different advance angle values. To drive the first motor Ma and the second motor Mb in the step driving mode (open-loop driving mode), the energization state of the coil is switched at predetermined time intervals. To drive the first motor Ma and the second motor Mb in the feed-back driving mode, the energization state of the coil is switched in accordance with an output of a positional sensor.

The detailed configuration of each of the first motor Ma and the second motor Mb is described below.

FIG. 12 is a timing chart for describing operations of the shutter unit 20 when the camera 100 is operating in continuous shooting mode. FIGS. 3 to 11 are illustrations for describing the states of the shutter unit 20 in A to I statuses illustrated in FIG. 12.

The shutter unit 20 according to the present embodiment performs a first-frame shooting operation from the A status to H status illustrated in FIG. 12. In the first-frame shooting operation, the first shutter driving mechanism functions as a leading blade, and the second shutter driving mechanism functions as a trailing blade. The shutter unit 20 according to the present embodiment performs a second-frame shooting operation from the H status to I status illustrated in FIG. 12. In the second-frame shooting operation, the second shutter driving mechanism functions as the leading blade, and the second shutter driving mechanism functions as the trailing blade. In a third-frame shooting operation, the first shutter driving

mechanism functions as the leading blade, and the second shutter driving mechanism functions as the trailing blade.

When the camera **100** starts a shooting operation, it is in A status illustrated in FIG. 12. FIGS. 3A and 3B are illustrations for describing a state of the shutter unit **20** in A status. FIG. 3A is an illustration for describing the state of the first shutter driving mechanism. FIG. 3B is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. 3A, in A status, the first blade **110** opens the aperture **105a**. In the state illustrated in FIG. 3A, the protruding section **107a** in the first rotor plate **107** is in contact with the left arm section of the first spring **108**. However, in this state, the first spring **108** is not charged and is in its natural state.

As illustrated in FIG. 3B, in A status, the second blade **120** opens the aperture **105a**. At this time, the protruding section **117a** in the second rotor plate **117** is in contact with the right arm section of the second spring **118**. However, in this state, the second spring **118** is not charged and is in its natural state.

As illustrated in FIG. 12, in A status, the control circuit **13** controls the driving circuit **14a** such that the first motor Ma is driven clockwise in feed-back driving mode with low advance angle. In A status, the control circuit **13** controls the driving circuit **14b** such that the second motor Mb is not driven in any direction. Thus the shutter unit **20** moves to the B status illustrated in FIG. 12.

FIGS. 4A and 4B are illustrations for describing a state of the shutter unit **20** in B status. FIG. 4A is an illustration for describing the state of the first shutter driving mechanism. FIG. 4B is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. 4A, in B status, the first blade **110** closes the aperture **105a**. As illustrated in FIG. 12, in the period from the A status to B status, the first motor Ma is driven clockwise in feed-back driving mode with low advance angle. Thus the first rotor plate **107** rotates counterclockwise from the state illustrated in FIG. 3A. Here, because the pinion gear **101** in the first motor Ma and the gear section **107b** in the first rotor plate **107** engage with each other, the rotation direction of the first motor Ma and that of the first rotor plate **107** are opposite.

When the first rotor plate **107** rotates counterclockwise from the state illustrated in FIG. 3A (A status), the first rotor plate **107** rotates while charging the first spring **108**. In this period, the first rotor plate **107** rotates counterclockwise while charging the first spring **108**, and thus variations in load during the driving of the first motor Ma are large. However, because the first motor Ma is driven in feed-back driving mode with low advance angle, the first motor Ma does not lose synchronization.

In the state illustrated in FIG. 4A (B status), because the first spring **108** is charged, the first rotor plate **107** is urged in a clockwise direction by the first spring **108**.

When the first rotor plate **107** rotates counterclockwise from the state illustrated in FIG. 3A (A status), the cam pin **109a** in the first driving lever **109** follows the first idle running driving region A in the cam groove **107c** in this period. Accordingly, the position of the first driving lever **109** in the state illustrated in FIG. 4A (B status) is substantially the same as the position of the first driving lever **109** in the state illustrated in FIG. 3A (A status).

The B status of the second shutter driving mechanism illustrated in FIG. 4B is the same as the A status of the second shutter driving mechanism illustrated in FIG. 3B. When the state moves from the A status to B status, the second motor Mb is not driven, and thus the second rotor plate **117** remains unchanged from the state illustrated in FIG. 3B (A status).

As illustrated in FIG. 12, in B status, the control circuit **13** controls the driving circuit **14a** such that the first motor Ma is driven counterclockwise in step driving mode. In B status, the control circuit **13** controls the driving circuit **14b** such that the second motor Mb is driven clockwise in feed-back driving mode with low advance angle. Thus the shutter unit **20** moves to the C status illustrated in FIG. 12. That is, in the present embodiment, the start of driving for an approach run in the second shutter driving mechanism lags behind the start of driving for an approach run in the first shutter driving mechanism by an exposure time t_1 .

The first shutter driving mechanism starts driving for an approach run in step driving mode in B status. In driving for the approach run, the control circuit **13** gradually increases the rotational speed of the first motor Ma by gradually reducing the width of a driving pulse. In driving for the approach run, the cam pin **109a** follows the first idle running driving region A in the cam groove **107c**, where the cam lift is substantially zero. Accordingly, in this period, because the first driving lever **109** does not virtually rotate even when the first rotor plate **107** is driven, variations in load during the driving of the first motor Ma are small. Thus when the first motor Ma is driven in step driving mode, the first motor Ma does not lose synchronization.

FIGS. 5A and 5B are illustrations for describing a state of the shutter unit **20** in C status. FIG. 5A is an illustration for describing the state of the first shutter driving mechanism. FIG. 5B is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. 5A, in C status, the first blade **110** closes the aperture **105a**. Because the first motor Ma is driven counterclockwise in the period from the B status to C status, the first rotor plate **107** is rotated clockwise by a combined force of the driving force of the first motor Ma and the urging force of the first spring **108**. The urging force of the first spring **108** is provided to the first rotor plate **107** up to the C status illustrated in FIG. 5A.

When the first rotor plate **107** rotates clockwise from the state illustrated in FIG. 4A (B status), the cam pin **109a** in the first driving lever **109** follows the first idle running driving region A in the cam groove **107c** in this period. Accordingly, the position of the first driving lever **109** in the state illustrated in FIG. 5A (C status) is substantially the same as the position of the first driving lever **109** in the state illustrated in FIG. 4A (B status).

As illustrated in FIG. 5B, in C status, the second blade **120** opens the aperture **105a**. In the period from the B status to C status, because the second motor Mb is driven clockwise in feed-back driving mode with low advance angle, the second rotor plate **117** rotates counterclockwise from the state illustrated in FIG. 4B. Here, because the pinion gear **111** in the second motor Mb and the gear section **117b** in the second rotor plate **117** engage with each other, the rotation direction of the second motor Mb and that of the second rotor plate **117** are opposite.

When the second rotor plate **117** rotates clockwise from the state illustrated in FIG. 4B (B status), the second rotor plate **117** rotates while charging the second spring **118**. In this period, the second rotor plate **117** rotates clockwise while charging the second spring **118**, and thus variations in load during the driving of the second motor Mb are large. However, because the second motor Mb is driven in feed-back driving mode with low advance angle, the second motor Mb does not lose synchronization.

In the state illustrated in FIG. 5B (C status), because the second spring **118** is charged, the second rotor plate **117** is urged in a clockwise direction by the second spring **118**.

When the second rotor plate **117** rotates clockwise from the state illustrated in FIG. **4B** (B status), the cam pin **119a** in the second driving lever **119** also follows the first idle running driving region A in the cam groove **117c** in this period. Accordingly, the position of the second driving lever **119** in the state illustrated in FIG. **5B** (C status) is substantially the same as the position of the second driving lever **119** in the state illustrated in FIG. **4B** (B status).

As illustrated in FIG. **12**, in C status, the control circuit **13** also controls the driving circuit **14a** such that the first motor Ma is driven counterclockwise in step driving mode. In C status, the control circuit **13** controls the driving circuit **14b** such that the second motor Mb is driven counterclockwise in step driving mode. Thus the shutter unit **20** moves to the D status illustrated in FIG. **12**. The second shutter driving mechanism starts driving for an approach run in step driving mode in C status. In driving for the approach run, the control circuit **13** gradually increases the rotational speed of the second motor Mb by gradually reducing the width of a driving pulse. In driving for the approach run, the cam pin **119a** follows the first idle running driving region A in the cam groove **117c**, where the cam lift is substantially zero. Thus when the second motor Mb is driven in step driving mode, the second motor Mb does not lose synchronization.

FIGS. **6A** and **6B** are illustrations for describing a state of the shutter unit **20** in D status. FIG. **6A** is an illustration for describing the state of the first shutter driving mechanism. FIG. **6B** is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. **6A**, the D status is a state immediately before the first blade **110** starts opening the aperture **105a**. Because the first motor Ma is driven counterclockwise in the period from the C status to D status, the first rotor plate **107** is rotated clockwise by the driving force of the first motor Ma.

When the first rotor plate **107** rotates clockwise from the state illustrated in FIG. **5A** (C status), the cam pin **109a** in the first driving lever **109** follows the first idle running driving region A in the cam groove **107c** in this period. Accordingly, the position of the first driving lever **109** in the state illustrated in FIG. **6A** (D status) is substantially the same as the position of the first driving lever **109** in the state illustrated in FIG. **5A** (C status).

As illustrated in FIG. **6B**, in D status, the second blade **120** opens the aperture **105a**. In the period from the C status to a state before the D status, because the second motor Mb is driven counterclockwise, the second rotor plate **117** is rotated clockwise by a combined force of the driving force of the second motor Mb and the urging force of the second spring **118**. The urging force of the second spring **118** is provided to the second rotor plate **117** up to the state before the D status illustrated in FIG. **6B**. That is, in D status illustrated in FIG. **6B**, the urging force of the second spring **118** is not provided to the second rotor plate **117**, and the second rotor plate **117** is rotated clockwise by only the driving force of the second motor Mb.

When the second rotor plate **117** rotates clockwise from the state illustrated in FIG. **5B** (C status), the cam pin **119a** in the second driving lever **119** also follows the first idle running driving region A in the cam groove **117c** in this period. Accordingly, the position of the second driving lever **119** in the state illustrated in FIG. **6B** (D status) is substantially the same as the position of the second driving lever **119** in the state illustrated in FIG. **5B** (C status).

As illustrated in FIG. **12**, in D status, the control circuit **13** controls the driving circuit **14a** such that the first motor Ma is driven counterclockwise in feed-back driving mode with high

advance angle. In D status, the control circuit **13** also controls the driving circuit **14b** such that the second motor Mb is driven counterclockwise in step driving mode. Thus the shutter unit **20** moves to the E status illustrated in FIG. **12**. The first shutter driving mechanism starts driving for exposure in feed-back driving mode with high advance angle in D status.

FIGS. **7A** and **7B** are illustrations for describing a state of the shutter unit **20** in E status. FIG. **7A** is an illustration for describing the state of the first shutter driving mechanism. FIG. **7B** is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. **7A**, in E status, the first blade **110** opens the aperture **105a**. Because the first motor Ma is driven counterclockwise in the period from the D status to E status, the first rotor plate **107** is rotated clockwise by the driving force of the first motor Ma.

When the first rotor plate **107** rotates clockwise from the state illustrated in FIG. **6A** (D status), the cam pin **109a** in the first driving lever **109** follows the exposure driving region B in the cam groove **107c** in this period. This causes the first blade **110** to open the closed aperture **105a**. Accordingly, in exposure driving, it is necessary to drive the first motor Ma at high speeds, and this leads to large variations in load during the driving of the first motor Ma. At this time, because the first motor Ma is driven in feed-back driving mode with high advance angle, the high-speed driving and the load variations do not cause the first motor Ma to lose synchronization. Because the rotation speed of the first motor Ma is sufficiently high due to the driving for the approach run, the first motor Ma can be driven in feed-back driving mode with high advance angle.

As illustrated in FIG. **7B**, the E status is a state immediately before the second blade **120** starts closing the aperture **105a**. In the period from the D status to E status, because the second motor Mb is driven counterclockwise, the second rotor plate **117** is rotated clockwise by the driving force of the second motor Mb.

When the second rotor plate **117** rotates clockwise from the state illustrated in FIG. **6B** (D status), the cam pin **119a** in the second driving lever **119** follows the first idle running driving region A in the cam groove **117c** in this period. Accordingly, the position of the second driving lever **119** in the state illustrated in FIG. **7B** (E status) is substantially the same as the position of the second driving lever **119** in the state illustrated in FIG. **6B** (D status).

As illustrated in FIG. **12**, in E status, the control circuit **13** controls the driving circuit **14a** such that the first motor Ma is driven counterclockwise in feed-back driving mode with high advance angle. In E status, the control circuit **13** also controls the driving circuit **14b** such that the second motor Mb is driven counterclockwise in feed-back driving mode with high advance angle. Thus the shutter unit **20** moves to the F status illustrated in FIG. **12**. The second shutter driving mechanism starts driving for exposure in feed-back driving mode with high advance angle in E status.

FIGS. **8A** and **8B** are illustrations for describing a state of the shutter unit **20** in F status. FIG. **8A** is an illustration for describing the state of the first shutter driving mechanism. FIG. **8B** is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. **8A**, in F status, the first blade **110** opens the aperture **105a**. Because the first motor Ma is driven counterclockwise in the period from the D status to E status, the first rotor plate **107** is rotated clockwise by the driving force of the first motor Ma.

When the first rotor plate **107** rotates clockwise from the state illustrated in FIG. **7A** (E status), the cam pin **109a** in the

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first driving lever **109** follows the second idle running driving region C in the cam groove **107c** in this period. Accordingly, the position of the first driving lever **109** in the state illustrated in FIG. 8A (F status) is substantially the same as the position of the first driving lever **109** in the state illustrated in FIG. 7A (E status).

As illustrated in FIG. 8B, in F status, the second blade **120** closes the aperture **105a**. In the period from the E status to F status, because the second motor Mb is driven counterclockwise, the second rotor plate **117** is rotated clockwise by the driving force of the second motor Mb.

When the second rotor plate **117** rotates clockwise from the state illustrated in FIG. 7B (E status), the cam pin **119a** in the second driving lever **119** follows the exposure driving region B in the cam groove **117c** in this period. This causes the second blade **120** to close the opened aperture **105a**. Accordingly, in exposure driving, it is necessary to drive the second motor Mb at high speeds, and this leads to large variations in load during the driving of the second motor Mb. At this time, because the second motor Mb is driven in feed-back driving mode with high advance angle, the high-speed driving and the load variations do not cause the second motor Mb to lose synchronization. Because the rotation speed of the second motor Mb is sufficiently high due to the driving for the approach run, the second motor Mb can be driven in feed-back driving mode with high advance angle.

As illustrated in FIG. 12, in F status, the control circuit **13** controls the driving circuit **14a** such that the first motor Ma is driven counterclockwise in feed-back driving mode with high advance angle. In F status, the control circuit **13** also controls the driving circuit **14b** such that the second motor Mb is driven counterclockwise in feed-back driving mode with high advance angle. Thus the shutter unit **20** moves to the G status illustrated in FIG. 12.

FIGS. 9A and 9B are illustrations for describing a state of the shutter unit **20** in G status. FIG. 9A is an illustration for describing the state of the first shutter driving mechanism. FIG. 9B is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. 9A, in G status, the first blade **110** opens the aperture **105a**. The first motor Ma is driven counterclockwise in the period from the F status to G status. In the period from the F status to G status, the protruding section **107a** in the first rotor plate **107** is in contact with the right arm section of the first spring **108**, and the first rotor plate **107** rotates clockwise while charging the first spring **108**. That is, the first spring **108** acts to apply a break to the clockwise rotation of the first rotor plate **107**. In the state illustrated in FIG. 9A, the first spring **108** is charged, and the first rotor plate **107** is urged in a counterclockwise direction by the first spring **108**.

When the first rotor plate **107** rotates clockwise from the state illustrated in FIG. 8A (F status), the cam pin **109a** in the first driving lever **109** follows the second idle running driving region C in the cam groove **107c** in this period. Accordingly, the position of the first driving lever **109** in the state illustrated in FIG. 9A (G status) is substantially the same as the position of the first driving lever **109** in the state illustrated in FIG. 8A (F status). In this period, the first rotor plate **107** rotates clockwise while charging the first spring **108**, and thus variations in load during the driving of the first motor Ma are large. However, because the first motor Ma is driven in feed-back driving mode with high advance angle, the first motor Ma does not lose synchronization.

As illustrated in FIG. 9B, in G status, the second blade **120** closes the aperture **105a**. In the period from the F status to G status, because the second motor Mb is driven counterclock-

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wise, the second rotor plate **117** is rotated clockwise by the driving force of the second motor Mb. In the state illustrated in FIG. 9B, the protruding section **117a** in the second rotor plate **117** is in contact with the left arm section of the second spring **118**. However, in this state, the second spring **118** is not charged and is in its natural state.

When the second rotor plate **117** rotates clockwise from the state illustrated in FIG. 8B (F status), the cam pin **119a** in the second driving lever **119** also follows the second idle running driving region C in the cam groove **117c** in this period. Accordingly, the position of the second driving lever **119** in the state illustrated in FIG. 9B (G status) is substantially the same as the position of the second driving lever **119** in the state illustrated in FIG. 8B (F status).

As illustrated in FIG. 12, in G status, the control circuit **13** controls the driving circuit **14a** such that current supply to the first motor Ma is held. Here, holding the current supply indicates maintaining the phase of the current supply to the coil of the first motor Ma in G status. In G status, the control circuit **13** also controls the driving circuit **14b** such that the second motor Mb is driven counterclockwise in feed-back driving mode with high advance angle. Thus the shutter unit **20** moves to the H status illustrated in FIG. 12.

FIGS. 10A and 10B are illustrations for describing a state of the shutter unit **20** in H status. FIG. 10A is an illustration for describing the state of the first shutter driving mechanism. FIG. 10B is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. 10A, in H status, the first blade **110** opens the aperture **105a**. Because the current supply to the first motor Ma is held in G status, the first motor Ma and the first rotor plate **107** remain in G status. That is, the state illustrated in FIG. 10A (H status) is the same as the state illustrated in FIG. 9A (G status).

As illustrated in FIG. 10B, in H status, the second blade **120** closes the aperture **105a**. In the period from the G status to H status, the second motor Mb is driven counterclockwise. In the period from the G status to H status, the protruding section **117a** in the second rotor plate **117** is in contact with the left arm section of the second spring **118**, and the second rotor plate **117** rotates clockwise while charging the second spring **118**. That is, the second spring **118** acts to apply a break to the clockwise rotation of the second rotor plate **117**. In the state illustrated in FIG. 10B, the second spring **118** is charged, and the second rotor plate **117** is urged in a counterclockwise direction by the second spring **118**.

When the second rotor plate **117** rotates clockwise from the state illustrated in FIG. 9B (G status), the cam pin **119a** in the second driving lever **119** follows the second idle running driving region C in the cam groove **117c** in this period. Accordingly, the position of the second driving lever **119** in the state illustrated in FIG. 10B (H status) is substantially the same as the position of the second driving lever **119** in the state illustrated in FIG. 9B (G status). In this period, the second rotor plate **117** rotates clockwise while charging the second spring **118**, and thus variations in load during the driving of the second motor Mb are large. However, because the second motor Mb is driven in feed-back driving mode with high advance angle, the second motor Mb does not lose synchronization.

As described above, the shutter unit **20** according to the present embodiment performs the first-frame shooting operation from the A status to H status illustrated in FIG. 12. In the first-frame shooting operation, the first shutter driving mechanism functions as the leading blade, and the second shutter driving mechanism functions as the trailing blade. In the second-frame shooting operation, the second shutter driv-

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ing mechanism functions as the leading blade, and the first shutter driving mechanism functions as the trailing blade. That is, in the first-frame shooting operation, the first shutter driving mechanism performs an exposure operation ahead of the second shutter driving mechanism. In the second-frame shooting operation, the second shutter driving mechanism performs an exposure operation ahead of the first shutter driving mechanism.

In the present embodiment, the start of driving for an approach run in the first shutter driving mechanism is caused to lag behind the start of driving for an approach run in the second shutter driving mechanism by an exposure time t_2 for the second frame by adjustment of the period of time for which the current supply to the first motor Ma is held.

As illustrated in FIG. 12, in H status, the control circuit 13 controls the driving circuit 14a such that the current supply to the first motor Ma is held. In H status, the control circuit 13 also controls the driving circuit 14b such that the second motor Mb is driven clockwise in step driving mode. Thus the second rotor plate 117 is rotated counterclockwise by the driving force of the second motor Mb and the urging force of the second spring 118. The second shutter driving mechanism starts driving for an approach run in step driving mode in H status. Thus the shutter unit 20 moves to the G' status illustrated in FIG. 12.

The state of the shutter unit 20 in G' status illustrated in FIG. 12 is the same as the state illustrated in FIGS. 9A and 9B.

As illustrated in FIG. 12, in G' status, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven clockwise in step driving mode. Thus the first rotor plate 107 is rotated counterclockwise by the driving force of the first motor Ma and the urging force of the first spring 108. The first shutter driving mechanism starts driving for an approach run in step driving mode in G' status. In G' status, the control circuit 13 controls the driving circuit 14b such that the second motor Mb is driven clockwise in step driving mode. Thus the shutter unit 20 moves to the F' status illustrated in FIG. 12.

The state of the shutter unit 20 in F' status illustrated in FIG. 12 is the same as the state illustrated in FIGS. 8A and 8B.

As illustrated in FIG. 12, in F' status, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven clockwise in step driving mode. In F' status, the control circuit 13 controls the driving circuit 14b such that the second motor Mb is driven clockwise in feed-back driving mode with high advance angle. Thus the shutter unit 20 moves to the E' status illustrated in FIG. 12. The second shutter driving mechanism starts driving for exposure in feed-back driving mode with high advance angle in F' status. Because the rotation speed of the second motor Mb is sufficiently high due to the driving for the approach run, the second motor Mb can be driven in feed-back driving mode with high advance angle.

The state of the shutter unit 20 in F' status illustrated in FIG. 12 is the same as the state illustrated in FIG. 8.

As illustrated in FIG. 12, in E' status, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven clockwise in feed-back driving mode with high advance angle. In E' status, the control circuit 13 controls the driving circuit 14b such that the second motor Mb is driven clockwise in feed-back driving mode with high advance angle. Thus the shutter unit 20 moves to the D' status illustrated in FIG. 12. The first shutter driving mechanism starts driving for exposure in feed-back driving mode with high advance angle in E' status. Because the rotation speed of the first motor Ma is sufficiently high due to the driving for the approach run, the first motor Ma can be driven in feed-back driving mode with high advance angle.

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The state of the shutter unit 20 in E' status illustrated in FIG. 12 is the same as the state illustrated in FIGS. 7A and 7B.

As illustrated in FIG. 12, in D' status, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven clockwise in feed-back driving mode with high advance angle. In D' status, the control circuit 13 controls the driving circuit 14b such that the second motor Mb is driven clockwise in feed-back driving mode with high advance angle. Thus the shutter unit 20 moves to the C' status illustrated in FIG. 12.

The state of the shutter unit 20 in C' status illustrated in FIG. 12 is the same as the state illustrated in FIGS. 6A and 6B.

As illustrated in FIG. 12, in C' status, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven clockwise in feed-back driving mode with high advance angle. In C' status, the control circuit 13 controls the driving circuit 14b such that the current supply to the second motor Mb is held. Here, holding the current supply indicates maintaining the phase of the current supply to the second motor Mb in D status. Thus the shutter unit 20 moves to the I status illustrated in FIG. 12.

FIGS. 11A and 11B are illustrations for describing a state of the shutter unit 20 in I status. FIG. 11A is an illustration for describing the state of the first shutter driving mechanism. FIG. 11B is an illustration for describing the state of the second shutter driving mechanism.

As illustrated in FIG. 11A, in I status, the first blade 110 closes the aperture 105a. As illustrated in FIG. 12, because the first motor Ma is driven clockwise in the period from the C' status to I status, the first rotor plate 107 is rotated counterclockwise from the state illustrated in FIG. 5A. In the period from the C' status to I status, the protruding section 107a in the first rotor plate 107 is in contact with the left arm section of the first spring 108, and the first rotor plate 107 rotates counterclockwise while charging the first spring 108. That is, the first spring 108 acts to apply a break to the counterclockwise rotation of the first rotor plate 107. In the state illustrated in FIG. 11A, the first spring 108 is charged, and the first rotor plate 107 is urged in a clockwise direction by the first spring 108.

As illustrated in FIG. 11B, in I status, the second blade 120 opens the aperture 105a. Because the current supply to the second motor Mb is held in C' status, the second motor Mb and the second rotor plate 117 remain in C' status. That is, the state illustrated in FIG. 5B is the same as the state illustrated in FIG. 11B.

As described above, the shutter unit 20 according to the present embodiment performs the second-frame shooting operation from the H status to I status illustrated in FIG. 12. In the second-frame shooting operation, the second shutter driving mechanism functions as the leading blade, and the first shutter driving mechanism functions as the trailing blade. In the third-frame shooting operation, the first shutter driving mechanism functions as the leading blade, and the second shutter driving mechanism functions as the trailing blade. In the present embodiment, the start of driving for an approach run in the second shutter driving mechanism is caused to lag behind the start of driving for an approach run in the first shutter driving mechanism by an exposure time t_3 for the third frame by adjustment of the period of time for which the current supply to the second motor Mb is held.

As illustrated in FIG. 12, in I status, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven counterclockwise in step driving mode. The control circuit 13 controls the driving circuit 14b such that the current supply to the second motor Mb is held. Thus the shutter unit 20 moves to the C status illustrated in FIG. 12.

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After that, the same shooting operation as that for the first frame is performed.

(Variation)

FIG. 13 is a timing chart for describing operations of the shutter unit 20 when the camera 100 is operating in continuous shooting mode as a variation of the present embodiment.

In the above-described embodiment, a lag between the leading blade and the trailing blade is produced by making the timing for starting the driving for the approach run in the shutter driving mechanism functioning as the leading blade and the timing for starting the driving for the approach run in the shutter driving mechanism functioning as the trailing blade different.

In contrast, in the variation, a lag between the leading blade and the trailing blade is produced by making a pulse rate for the driving for the approach run in the shutter driving mechanism functioning as the leading blade and a pulse rate for the driving for the approach run in the shutter driving mechanism functioning as the trailing blade different. That is, the pulse rate for the driving for the approach run in the shutter driving mechanism functioning as the leading blade is set at a value larger than the pulse rate for the driving for the approach run in the shutter driving mechanism functioning as the trailing blade. Thus even in the same approach run period, the time required for the driving for the approach run in the shutter driving mechanism functioning as the trailing blade is longer than the time required for the driving for the approach run in the shutter driving mechanism functioning as the leading blade.

In the variation, in A status illustrated in FIG. 13, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven clockwise in feed-back driving mode with low advance angle. In A status illustrated in FIG. 13, the control circuit 13 controls the driving circuit 14b such that the second motor Mb is driven clockwise in feed-back driving mode with low advance angle. Thus the shutter unit 20 moves to the I status illustrated in FIG. 13.

In I status illustrated in FIG. 13, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven counterclockwise in step driving mode. In I status illustrated in FIG. 13, the control circuit 13 controls the driving circuit 14b such that the second motor Mb is driven counterclockwise in step driving mode. Thus the shutter unit 20 moves to the D status illustrated in FIG. 13.

The state from the D status to G status illustrated in FIG. 13 is the same as that from the D status to G status illustrated in FIG. 12 in the embodiment described above.

In G status illustrated in FIG. 13, the control circuit 13 also controls the driving circuit 14a such that the first motor Ma is driven counterclockwise in feed-back driving mode with high advance angle. In D status illustrated in FIG. 13, the control circuit 13 also controls the driving circuit 14b such that the second motor Mb is driven counterclockwise in feed-back driving mode with high advance angle.

In the above-described embodiment, in G status illustrated in FIG. 12, the control circuit 13 controls the driving circuit 14a such that the current supply to the first motor Ma is held. In the variation, the control circuit 13 controls the driving circuit 14a such that the first motor Ma is driven counterclockwise in feed-back driving mode with high advance angle. Accordingly, although the first rotor plate 107 tries to rotate clockwise, because the protruding section 107a in the first rotor plate 107 comes into contact with the stopper on the cover plate 103, the clockwise rotation of the first rotor plate 107 is blocked.

The characteristics in the variation are substantially the same as those in the above-described embodiment, except for

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the method of producing a lag between the leading blade and the trailing blade and the respect in which holding the current supply is not performed.

Next, the details of the first motor Ma and the second motor Mb are described with reference to FIGS. 14 to 16.

FIG. 14 illustrates a motor 1 used as each of the first motor Ma and the second motor Mb. For the sake of the description, parts of some components are removed in the illustration.

As illustrated in FIG. 14, a rotor 3 includes a magnet 2 and is rotatably controlled by the control circuit (controller) 13 and the driving circuit 14. The magnet 2 is cylindrical, has a circumferential surface divided in its circumferential direction, and is multipole-magnetized in different poles in an alternately manner. In the present embodiment, the magnet 2 is divided in eight elements, that is, magnetized in eight poles. The number of divisions is not limited to eight. The magnet 2 may be magnetized in four or twelve poles.

A first coil 4 is arranged on a first end of the magnet 2 in its axial direction.

A first yoke 6 is made of a soft magnetic material and is opposed to the circumferential surface of the magnet 2 such that a gap is present therebetween. The first yoke 6 axially extends from an annular main body portion and includes a plurality of first magnetic pole sections 6a arranged at predetermined intervals in its circumferential direction. The first magnetic pole sections 6a are excited by energization of the first coil 4.

The first coil 4, the first yoke 6, and the magnet 2 opposed to the plurality of first magnetic pole sections 6a constitute a first stator unit.

A second coil 5 is arranged on a second end of the magnet 2 in its axial direction, and the second end is opposite to the first end on which the first coil 4 is arranged.

A second yoke 7 is made of a soft magnetic material and is opposed to the circumferential surface of the magnet 2 such that a gap is present therebetween. The second yoke 7 axially extends from the annular main body portion and includes a plurality of second magnetic pole sections 7a arranged at predetermined intervals in its circumferential direction. The second magnetic pole sections 7a are excited by energization of the second coil 5.

The second coil 5, the second yoke 7, and the magnet 2 opposed to the plurality of second magnetic pole sections 7a constitute a second stator unit.

A torque provided to the rotor 3 can be changed by switching the magnetized polarity (north pole, south pole) of each of the first magnetic pole sections 6a and the second magnetic pole sections 7a.

A first magnetic sensor (first detecting element) 8, a second magnetic sensor (second detecting element) 9, a third magnetic sensor (third detecting element) 10, and a fourth magnetic sensor (fourth detecting element) 11 constitute detecting means. Each of the magnetic sensors is a Hall element configured to detect a magnetic flux of the magnet 2 and is fixed to a motor cover 12.

The motor cover 12 fixes and retains the first yoke 6 and the second yoke 7 such that the first magnetic pole sections 6a and the second magnetic pole sections 7a are displaced with respect to a magnetization phase of the magnet 2 by approximately 90 degrees in electrical angle.

Here, the electrical angle is an angle represented based on the assumption that one cycle of the magnetic force of the magnet is 360°. The electrical angle θ can be expressed by the following equation:

$$\theta = 60 \times M/2$$

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where M is the number of poles of the rotor, and the mechanical angle is θ_0 .

In the present embodiment, the magnet 2 is magnetized in eight poles, and 90 degrees in electrical angle is 22.5 degrees in mechanical angle.

The control circuit 13 can switch the driving among the step driving and the two kinds of feed-back driving with different amounts of the advance angle. In step driving, the control circuit 13 controls the driving circuit 14 such that the energization state of the first coil 4 and the second coil 5 is switched at predetermined time intervals. That is, in step driving, none of outputs of the first magnetic sensor 8, the second magnetic sensor 9, the third magnetic sensor 10, and the fourth magnetic sensor 11 are used.

A case where the control circuit 13 performs the feed-back driving is described below. When the control circuit 13 performs the two kinds of feed-back driving, outputs of the first magnetic sensor 8, the second magnetic sensor 9, the third magnetic sensor 10, and the fourth magnetic sensor 11 are used.

In the present embodiment, even in switching the energization direction, a large rotational driving force is obtainable by arranging each magnetic sensor in a positional relationship with respect to each yoke described below.

FIGS. 15A to 15I are illustrations for describing operations of the motor 1. Actual operations of the motor 1 are described with reference to FIGS. 15A to 15I. The state in FIG. 15A is described as an initial state in driving.

(1) Clockwise Driving

(1-i) Low Advance Angle Driving (First Energization Mode)

The clockwise driving mode with low advance angle is described. The driving mode with low advance angle can achieve larger torque than that in the driving mode with high advance angle described below.

In the clockwise driving mode with low advance angle, the rotor 3 is rotated clockwise by switching excitation of each of the first magnetic pole sections 6a in response to an output signal of the first magnetic sensor 8 and switching excitation of each of the second magnetic pole sections 7a in response to an output signal of the second magnetic sensor 9. The direction of the clockwise rotation of the rotor 3 corresponds to a first rotation direction.

In this driving mode, the energization direction of each of the first coil 4 and the second coil 5 is switched using combinations described below.

When the first magnetic sensor 8 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the north pole. When the first magnetic sensor 8 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the south pole.

When the second magnetic sensor 9 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the south pole. When the second magnetic sensor 9 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the north pole.

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In the state illustrated in FIG. 15A, both the first magnetic sensor 8 and the second magnetic sensor 9 detect the south pole of the magnet 2. At this time, the control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the north pole and the second magnetic pole section 7a is magnetized with the south pole. This produces a clockwise rotation force in the rotor 3 and the magnet 2.

When the rotor 3 rotates clockwise from the state illustrated in FIG. 15A, the center Q1 of each of the south poles of the magnet 2 and the center of the corresponding first magnetic pole section 6a are opposed to each other, as illustrated in FIG. 15B.

When the rotor 3 rotates clockwise from the state illustrated in FIG. 15B, the distance between the center Q1 of the south pole of the magnet 2 and the first magnetic pole section 6a is the same as the distance between the center Q2 of each of the north poles of the magnet 2 and the corresponding second magnetic pole section 7a, as illustrated in FIG. 15C.

The first magnetic sensor 8 is arranged such that when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the first magnetic sensor 8, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 0 degree to 45 degrees.

The first magnetic sensor 8 detects the north pole of the magnet 2 (switching from the south pole to north pole) between the state illustrated in FIG. 15B and the state illustrated in FIG. 15C. At this time, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the south pole. Because the second magnetic sensor 9 detects the south pole of the magnet 2 between the state illustrated in FIG. 15B and the state illustrated in FIG. 15C, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the south pole. This produces the clockwise rotation force in the rotor 3 and the magnet 2.

When the rotor 3 rotates clockwise from the state illustrated in FIG. 15C, the center Q2 of the north pole of the magnet 2 and the center of the second magnetic pole section 7a are opposed to each other, as illustrated in FIG. 15D.

When the rotor 3 rotates clockwise from the state illustrated in FIG. 15D, the distance between the center Q2 of the north pole of the magnet 2 and the first magnetic pole section 6a is the same as the distance between the center Q2 of the north pole of the magnet 2 and the second magnetic pole section 7a, as illustrated in FIG. 15E.

The second magnetic sensor 9 is arranged such that when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the second magnetic sensor 9, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 0 degree to 45 degrees.

The second magnetic sensor 9 detects the north pole of the magnet 2 (switching from the south pole to north pole) between the state illustrated in FIG. 15D and the state illustrated in FIG. 15E. At this time, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the north pole. Because the first magnetic sensor 8 detects the north pole of the magnet 2 between the state illustrated in FIG. 15D and the state illustrated in FIG. 15E, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the south pole. This produces the clockwise rotation force in the rotor 3 and the magnet 2.

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As described above, in the clockwise driving mode with low advance angle, the energization of the first coil 4 and the second coil 5 is sequentially switched by the outputs of the first magnetic sensor 8 and the second magnetic sensor 9, and the rotor 3 and the magnet 2 rotate in a clockwise direction.

When the rotor 3 rotates clockwise and the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the first magnetic sensor 8, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 0 degree to 45 degrees. That is, the first magnetic sensor 8 is arranged in a position where the amount of the advance angle from the position of the electrical advance angle 0 degree from the excitation switching timing at the first magnetic pole section 6a is smaller than the amount of the lag angle from the position of the electrical advance angle 90 degrees from the excitation switching timing at the first magnetic pole section 6a.

When the rotor 3 rotates clockwise and the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the second magnetic sensor 9, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 0 degree to 45 degrees. That is, the second magnetic sensor 9 is arranged in a position where the amount of the advance angle from the position of the electrical advance angle 0 degree from the excitation switching timing at the second magnetic pole section 7a is smaller than the amount of the lag angle from the position of the electrical advance angle 90 degrees from the excitation switching timing at the second magnetic pole section 7a.

(1-ii) High Advance Angle Driving (Second Energization Mode)

The clockwise driving mode with high advance angle is described. The driving mode with high advance angle can achieve higher speed rotation than that in the above-described driving mode with low advance angle.

In the clockwise driving mode with high advance angle, the rotor 3 is rotated clockwise by switching the magnetized polarity of the first magnetic pole section 6a in response to the output of the third magnetic sensor 10 and switching the magnetized polarity of the second magnetic pole section 7a in response to the output of the fourth magnetic sensor 11.

In this driving mode, the energization direction of each of the first coil 4 and the second coil 5 is switched using combinations described below.

When the third magnetic sensor 10 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the north pole. When the third magnetic sensor 10 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the south pole.

When the fourth magnetic sensor 11 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the south pole. When the fourth magnetic sensor 11 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13.

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The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the north pole.

In the state illustrated in FIG. 15A, both the third magnetic sensor 10 and the fourth magnetic sensor 11 detect the south pole of the magnet 2. Accordingly, when the first magnetic pole section 6a is magnetized with the north pole and the second magnetic pole section 7a is magnetized with the south pole, a clockwise rotation force is produced in the rotor 3 and the magnet 2.

When the rotor 3 rotates clockwise from the state illustrated in FIG. 15A, the center Q1 of each of the south poles of the magnet 2 and the center of the corresponding first magnetic pole section 6a are opposed to each other, as illustrated in FIG. 15B.

The third magnetic sensor 10 is arranged such that when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the third magnetic sensor 10, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 45 degrees to 90 degrees.

The third magnetic sensor 10 detects the north pole of the magnet 2 (switching from the south pole to north pole) between the state illustrated in FIG. 15A and the state illustrated in FIG. 15B. At this time, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the south pole. Because the fourth magnetic sensor 11 detects the south pole of the magnet 2 between the state illustrated in FIG. 15A and the state illustrated in FIG. 15B, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the south pole. This produces the clockwise rotation force in the rotor 3 and the magnet 2.

When the rotor 3 rotates clockwise from the state illustrated in FIG. 15B, the state moves to the state illustrated in FIG. 15C, and then the center Q2 of the north pole of the magnet 2 and the center of the second magnetic pole section 7a are opposed to each other, as illustrated in FIG. 15D.

The fourth magnetic sensor 11 is arranged such that when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the fourth magnetic sensor 11, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 45 degrees to 90 degrees.

The fourth magnetic sensor 11 detects the north pole of the magnet 2 (switching from the south pole to north pole) between the state illustrated in FIG. 15C and the state illustrated in FIG. 15D. At this time, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the north pole. Because the third magnetic sensor 10 detects the north pole of the magnet 2 between the state illustrated in FIG. 15C and the state illustrated in FIG. 15D, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the south pole. This produces the clockwise rotation force in the rotor 3 and the magnet 2.

As described above, in the clockwise driving mode with high advance angle, the energization of the first coil 4 and the second coil 5 is sequentially switched by the outputs of the third magnetic sensor 10 and the fourth magnetic sensor 11, and the rotor 3 and the magnet 2 rotate in a clockwise direction.

When the rotor 3 rotates clockwise and the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the third magnetic sensor 10, the

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excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 45 degrees to 90 degrees. That is, the third magnetic sensor 10 is arranged in a position where the amount of the advance angle from the position of the electrical advance angle 0 degree from the excitation switching timing at the first magnetic pole section 6a is larger than the amount of the lag angle from the position of the electrical advance angle 90 degrees from the excitation switching timing at the first magnetic pole section 6a.

When the rotor 3 rotates clockwise and the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the fourth magnetic sensor 11, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 45 degrees to 90 degrees. That is, the fourth magnetic sensor 11 is arranged in a position where the amount of the advance angle from the position of the electrical advance angle 0 degree from the excitation switching timing at the second magnetic pole section 7a is larger than the amount of the lag angle from the position of the electrical advance angle 90 degrees from the excitation switching timing at the second magnetic pole section 7a.

(2) Counterclockwise Driving

(2-i) Low Advance Angle Driving (Third Energization Mode)

The counterclockwise driving mode with low advance angle is described. Even for the counterclockwise rotation, the driving mode with low advance angle can achieve larger torque than that in the driving mode with high advance angle.

In the counterclockwise driving mode with low advance angle, the rotor 3 is rotated counterclockwise by switching excitation of each of the first magnetic pole sections 6a in response to an output signal of the third magnetic sensor 10 and switching excitation of each of the second magnetic pole sections 7a in response to an output signal of the fourth magnetic sensor 11. The direction of the counterclockwise rotation of the rotor 3 corresponds to a second rotation direction opposite to the first rotation direction.

In this driving mode, the energization direction of each of the first coil 4 and the second coil 5 is switched using combinations described below.

When the third magnetic sensor 10 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the south pole. When the third magnetic sensor 10 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the north pole.

When the fourth magnetic sensor 11 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the north pole. When the fourth magnetic sensor 11 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the south pole.

In the state illustrated in FIG. 15A, both the third magnetic sensor 10 and the fourth magnetic sensor 11 detect the south

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pole of the magnet 2. At this time, the control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the south pole and the second magnetic pole section 7a is magnetized with the north pole. This produces a counterclockwise rotation force in the rotor 3 and the magnet 2.

When the rotor 3 rotates counterclockwise from the state illustrated in FIG. 15A, the center Q1 of the south pole of the magnet 2 and the center of the second magnetic pole section 7a are opposed to each other, as illustrated in FIG. 15F.

When the rotor 3 rotates counterclockwise from the state illustrated in FIG. 15F, the distance between the center Q1 of the south pole of the magnet 2 and the second magnetic pole section 7a is the same as the distance between the center Q3 of the north pole of the magnet 2 and the first magnetic pole section 6a, as illustrated in FIG. 15G.

The fourth magnetic sensor 11 is arranged such that when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the fourth magnetic sensor 11, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 0 degree to 45 degrees.

The north pole of the magnet 2 (switching from the south pole to north pole) is detected between the state illustrated in FIG. 15F and the state illustrated in FIG. 15G. At this time, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the south pole. Because the third magnetic sensor 10 detects the south pole of the magnet 2 between the state illustrated in FIG. 15F and the state illustrated in FIG. 15G, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the south pole. This produces the counterclockwise rotation force in the rotor 3 and the magnet 2.

When the rotor 3 rotates counterclockwise from the state illustrated in FIG. 15G, the center Q3 of the north pole of the magnet 2 and the center of the first magnetic pole section 6a are opposed to each other, as illustrated in FIG. 15H.

When the rotor 3 rotates counterclockwise from the state illustrated in FIG. 15H, the distance between the center Q3 of the north pole of the magnet 2 and the first magnetic pole section 6a is the same as the distance between the center Q3 of the north pole of the magnet 2 and the second magnetic pole section 7a, as illustrated in FIG. 15I.

The third magnetic sensor 10 is arranged such that when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the third magnetic sensor 10, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 0 degree to 45 degrees.

The third magnetic sensor 10 detects the north pole of the magnet 2 (switching from the south pole to north pole) between the state illustrated in FIG. 15H and the state illustrated in FIG. 15I. At this time, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the north pole. Because the fourth magnetic sensor 11 detects the north pole of the magnet 2 between the state illustrated in FIG. 15H and the state illustrated in FIG. 15I, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the south pole. This produces the counterclockwise rotation force in the rotor 3 and the magnet 2.

As described above, in the counterclockwise driving mode with low advance angle, the energization of the first coil 4 and the second coil 5 is sequentially switched by the outputs of the

third magnetic sensor 10 and the fourth magnetic sensor 11, and the rotor 3 and the magnet 2 rotate in a counterclockwise direction.

When the rotor 3 rotates counterclockwise and the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the third magnetic sensor 10, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 0 degree to 45 degrees.

When the rotor 3 rotates counterclockwise and the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the fourth magnetic sensor 11, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 0 degree to 45 degrees.

(2-ii) High Advance Angle Driving (Fourth Energization Mode)

The counterclockwise driving mode with high advance angle is described. Even for the counterclockwise rotation, the driving mode with high advance angle can achieve higher speed rotation than that in the above-described driving mode with low advance angle.

In the counterclockwise driving mode with high advance angle, the rotor 3 is rotated counterclockwise by switching excitation of each of the first magnetic pole sections 6a in response to an output signal of the first magnetic sensor 8 and switching excitation of each of the second magnetic pole sections 7a in response to an output signal of the second magnetic sensor 9.

In this driving mode, the energization direction of each of the first coil 4 and the second coil 5 is switched using combinations described below.

When the first magnetic sensor 8 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the south pole. When the first magnetic sensor 8 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the first magnetic pole section 6a is magnetized with the north pole.

When the second magnetic sensor 9 detects the south pole of the magnet 2 (switching from the north pole to south pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the north pole. When the second magnetic sensor 9 detects the north pole of the magnet 2 (switching from the south pole to north pole), its detection signal is input into the control circuit 13. The control circuit 13 controls the driving circuit 14 such that the second magnetic pole section 7a is magnetized with the south pole.

In the state illustrated in FIG. 15A, both the first magnetic sensor 8 and the second magnetic sensor 9 detect the south pole of the magnet 2. Accordingly, when the first magnetic pole section 6a is magnetized with the south pole and the second magnetic pole section 7a is magnetized with the north pole, the counterclockwise rotation force is produced in the rotor 3 and the magnet 2.

When the rotor 3 rotates counterclockwise from the state illustrated in FIG. 15A, the center Q1 of the south pole of the magnet 2 and the center of the second magnetic pole section 7a are opposed to each other, as illustrated in FIG. 15F.

The second magnetic sensor 9 is arranged such that when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the second magnetic sensor 9, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 45 degrees to 90 degrees.

The second magnetic sensor 9 detects the north pole of the magnet 2 (switching from the south pole to north pole) between the state illustrated in FIG. 15A and the state illustrated in FIG. 15F. At this time, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the north pole. Because the first magnetic sensor 8 detects the south pole of the magnet 2 between the state illustrated in FIG. 15A and the state illustrated in FIG. 15F, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the south pole. This produces the counterclockwise rotation force in the rotor 3 and the magnet 2.

When the rotor 3 rotates counterclockwise from the state illustrated in FIG. 15F, the state moves to the state illustrated in FIG. 15G, and then the center Q3 of the north pole of the magnet 2 and the center of the first magnetic pole section 6a are opposed to each other, as illustrated in FIG. 15H.

The first magnetic sensor 8 is arranged such that when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the first magnetic sensor 8, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 45 degrees to 90 degrees.

The first magnetic sensor 8 detects the north pole of the magnet 2 (switching from the south pole to north pole) between the state illustrated in FIG. 15G and the state illustrated in FIG. 15H. At this time, the driving circuit 14 energizes the first coil 4 such that the first magnetic pole section 6a is magnetized with the north pole. Because the second magnetic sensor 9 detects the north pole of the magnet 2 between the state illustrated in FIG. 15G and the state illustrated in FIG. 15H, the driving circuit 14 energizes the second coil 5 such that the second magnetic pole section 7a is magnetized with the south pole. This produces the counterclockwise rotation force in the rotor 3 and the magnet 2.

As described above, in the counterclockwise driving mode with high advance angle, the energization of the first coil 4 and the second coil 5 is sequentially switched by the outputs of the first magnetic sensor 8 and the second magnetic sensor 9, and the rotor 3 and the magnet 2 rotate in a counterclockwise direction.

When the rotor 3 rotates counterclockwise and the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the first magnetic sensor 8, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 45 degrees to 90 degrees.

When the rotor 3 rotates counterclockwise and the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the second magnetic sensor 9, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between angle 45 degrees to 90 degrees.

FIGS. 16A to 16D are illustrations for describing positions in which the first magnetic sensor 8, the second magnetic sensor 9, the third magnetic sensor 10, and the fourth magnetic sensor 11 are arranged. As illustrated in FIGS. 16A to

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16D, the first magnetic sensor 8 in the motor 1 according to the present embodiment is arranged in a position that satisfies the following conditions.

(a) In the clockwise driving, when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the first magnetic sensor 8, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 0 degree and 45 degrees (see FIG. 16A).

(b) In the counterclockwise driving, when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the first magnetic sensor 8, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 45 degrees and 90 degrees (see FIG. 16C).

The second magnetic sensor 9 in the motor 1 according to the present embodiment is arranged in a position that satisfies the following conditions.

(c) In the clockwise driving, when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the second magnetic sensor 9, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 0 degree and 45 degrees (see FIG. 16B).

(d) In the counterclockwise driving, when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the second magnetic sensor 9, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 45 degrees and 90 degrees (see FIG. 16D).

The third magnetic sensor 10 in the motor 1 according to the present embodiment is arranged in a position that satisfies the following conditions.

(e) In the clockwise driving, when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the third magnetic sensor 10, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 45 degrees and 90 degrees (see FIG. 16A).

(f) In the counterclockwise driving, when the magnetized polarity of the first magnetic pole section 6a is switched on the basis of the output of the third magnetic sensor 10, the excitation switching timing for the first magnetic pole section 6a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 0 degree and 45 degrees (see FIG. 16C).

The fourth magnetic sensor 11 in the motor 1 according to the present embodiment is arranged in a position that satisfies the following conditions.

(g) In the clockwise driving, when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the fourth magnetic sensor 11, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3 corresponds to an electrical advance angle between 45 degrees and 90 degrees (see FIG. 16B).

(h) In the counterclockwise driving, when the magnetized polarity of the second magnetic pole section 7a is switched on the basis of the output of the fourth magnetic sensor 11, the excitation switching timing for the second magnetic pole section 7a with respect to the rotation position of the rotor 3

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corresponds to an electrical advance angle between 0 degree and 45 degrees (see FIG. 16D).

In the present embodiment, in consideration of errors in magnetization of magnets, errors in dimensions of sensors, errors of yokes, each magnetic sensor is arranged in a range described below.

The first magnetic sensor 8 is arranged in a range where the excitation switching timing for the first magnetic pole section 6a in the clockwise driving corresponds to an electrical advance angle between 14.4 degrees and 33.6 degrees and the excitation switching timing for the first magnetic pole section 6a in the counterclockwise driving corresponds to an electrical advance angle between 56.4 degrees and 75.6 degrees.

The second magnetic sensor 9 is arranged in a range where the excitation switching timing for the second magnetic pole section 7a in the clockwise driving corresponds to an electrical advance angle between 14.4 degrees and 33.6 degrees and the excitation switching timing for the second magnetic pole section 7a in the counterclockwise driving corresponds to an electrical advance angle between 56.4 degrees and 75.6 degrees.

The third magnetic sensor 10 is arranged in a range where the excitation switching timing for the first magnetic pole section 6a in the clockwise driving corresponds to an electrical advance angle between 56.4 degrees and 75.6 degrees and the excitation switching timing for the first magnetic pole section 6a in the counterclockwise driving corresponds to an electrical advance angle between 14.4 degrees and 33.6 degrees.

The fourth magnetic sensor 11 is arranged in a range where the excitation switching timing for the second magnetic pole section 7a in the clockwise driving corresponds to an electrical advance angle between 56.4 degrees and 75.6 degrees and the excitation switching timing for the second magnetic pole section 7a in the counterclockwise driving corresponds to an electrical advance angle between 14.4 degrees and 33.6 degrees.

The midpoint of a line segment connecting the first magnetic sensor 8 and the third magnetic sensor 10 corresponds to the electrical advance angle 45 degrees at the excitation switching timing for the first magnetic pole section 6a. The midpoint of a line segment connecting the second magnetic sensor 9 and the fourth magnetic sensor 11 corresponds to the electrical advance angle 45 degrees at the excitation switching timing for the second magnetic pole section 7a. This reduces variations in driving characteristics between the clockwise driving and the counterclockwise driving in the present embodiment.

The present embodiment uses a sensor unit in which the first magnetic sensor 8 and the third magnetic sensor 10 constitute a single unit and the second magnetic sensor 9 and the fourth magnetic sensor 11 constitute a single unit. In this case, in the clockwise driving, the first magnetic sensor 8 is in the position where the excitation switching timing for the first magnetic pole section 6a corresponds to the electrical advance angle 21 degrees, and the third magnetic sensor 10 is in the position where the excitation switching timing for the first magnetic pole section 6a corresponds to the electrical advance angle 69 degrees. In the clockwise driving, the second magnetic sensor 9 is in the position where the excitation switching timing for the second magnetic pole section 7a corresponds to the electrical advance angle 21 degrees, and the fourth magnetic sensor 11 is in the position where the excitation switching timing for the second magnetic pole section 7a corresponds to the electrical advance angle 69 degrees.

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The present invention can provide a shutter device in which, when a driven member is driven by a stepping motor and thus a light shielding member moves from a closed state to an open state or from the open state to the closed state, a stepping motor does not lose synchronization.

While the present invention has been described with reference to exemplary embodiments, it is to be understood that the invention is not limited to the disclosed exemplary embodiments. The scope of the following claims is to be accorded the broadest interpretation so as to encompass all such modifications and equivalent structures and functions.

This application claims the benefit of International Patent Application No. PCT/JP2013/080757, filed Nov. 14, 2013, which is hereby incorporated by reference herein in its entirety.

The invention claimed is:

1. A shutter device comprising:

a stepping motor configured to be driven in open-loop driving mode at which an energization state of a coil is switched at predetermined time intervals and in feed-back driving mode at which the energization state of the coil is switched in accordance with a rotation position of a rotor;

a driven member configured to be driven by the stepping motor; and

a light shielding member configured to travel between a closed state in which an aperture is closed and an open state in which the aperture is open,

wherein the light shielding member is driven by the driven member,

wherein the driven member is configured to provide a first driven zone and a second driven zone,

wherein in a case where the driven member is driven in the first driven zone, the light shielding member maintains the closed state or the open state,

wherein in a case where the driven member is driven in the second driven zone, the light shielding member travels from the closed state to the open state or from the open state to the closed state,

wherein the driven member is driven in the first driven zone by the stepping motor in one direction, and after the driven member is driven in the first driven zone, the driven member is driven in the second driven zone,

wherein in a case where the driven member is driven in the first driven zone, the stepping motor drives the driven member in the open-loop driving mode, and

wherein in a case where the driven member is driven in the second driven zone, the stepping motor drives the driven member in the feed-back driving mode.

2. The shutter device according to claim 1, wherein the driven member has a cam groove,

wherein the light shielding member has a follower portion which follows the cam groove,

wherein the cam groove has a first cam region and a second cam region,

wherein in a case where the follower portion follows the first cam region, the light shielding member maintains the closed state or the open state, and

wherein in a case where the follower portion follows the second cam region, the light shielding member travels from the closed state to the open state or from the open state to the closed state.

3. The shutter device according to claim 2, wherein the driven member is a rotating member, and

wherein the rotating member includes a circumferential portion to which a weight is fixed.

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4. The shutter device according to claim 1, further comprising: an urging member configured to urge the driven member,

wherein before the driven member is driven in the first driven zone, the stepping motor charges the urging member by driving the driven member in the feed-back driving mode, and

wherein in a case where the driven member is driven in the first driven zone, the urging member urges the driven member.

5. The shutter device according to claim 4, wherein the stepping motor is configured to be driven in first feed-back driving at which an advance angle value is low and in second feed-back driving at which the advance angle value is high,

wherein before the driven member is driven in the first driven zone, the stepping motor charges the urging member by driving the driven member in the first feed-back driving mode, and

wherein in a case where the driven member is driven in the second driven zone, the stepping motor drives the driven member in the second feed-back driving mode.

6. The shutter device according to claim 5, wherein the driven member has a third zone,

wherein the driven member is driven in the second driven zone by the stepping motor in one direction, and after the driven member is driven in the second driven zone, the driven member is driven in the third driven zone,

wherein in a case where the driven member is driven in the third driven zone, the light shielding member maintains the closed state or the open state, and

wherein in a case where the driven member is driven in the third driven zone, the stepping motor charges the urging member by driving the driven member in the second feed-back driving mode.

7. The shutter device according to claim 6, wherein after the driven member is driven in the third driven zone and the urging member is charged, the stepping motor holds a current supply.

8. An image pickup apparatus comprising a shutter device, the shutter device comprising:

a stepping motor configured to be driven in open-loop driving mode at which an energization state of a coil is switched at predetermined time intervals and in feed-back driving mode at which the energization state of the coil is switched in accordance with a rotation position of a rotor;

a driven member configured to be driven by the stepping motor; and

a light shielding member configured to travel between a closed state in which an aperture is closed and an open state in which the aperture is open,

wherein the light shielding member is driven by the driven member,

wherein the driven member is configured to provide a first driven zone and a second driven zone,

wherein in a case where the driven member is driven in the first driven zone, the light shielding member maintains the closed state or the open state,

wherein in a case where the driven member is driven in the second driven zone, the light shielding member travels from the closed state to the open state or from the open state to the closed state,

wherein the driven member is driven in the first driven zone by the stepping motor in one direction, and after the driven member is driven in the first driven zone, the driven member is driven in the second driven zone,

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wherein in a case wherein the driven member is driven in the first driven zone, the stepping motor drives the driven member in the open-loop driving mode, and
 wherein in a case where the driven member is driven in the second driven zone, the stepping motor drives the driven member in the feed-back driving mode.

9. The image pickup apparatus according to claim 8, wherein the driven member has a cam groove, wherein the light shielding member has a follower portion which follows the cam groove, wherein the cam groove has a first cam region and a second cam region, wherein in a case where the follower portion follows the first cam region, the light shielding member maintains the closed state or the open state, wherein in a case where the follower portion follows the second cam region, the light shielding member travels from the closed state to the state or from the open state to the closed state.

10. The image pickup apparatus according to claim 9, wherein the driven member is a rotating member, and wherein the rotating member includes a circumferential portion to which a weight is fixed.

11. The image pickup apparatus according to claim 8, wherein the shutter device comprises:

an urging member configured to urge the driven member, wherein before the driven member is driven in the first driven zone, the stepping motor charges the urging member by driving the driven member in the feed-back driving mode, and

wherein in a case where the driven member is driven in the first driven zone, the urging member urges the driven member.

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12. The image pickup apparatus according to claim 11, wherein the stepping motor is configured to be driven in first feed-back driving at which an advance angle value is low and in second feed-back driving at which the advance angle value is high,

wherein before the driven member is driven in the first driven zone, the stepping motor charges the urging member by driving the driven member in the first feed-back driving mode, and

wherein in a case where the driven member is driven in the second driven zone, the stepping motor drives the driven member in the second feed-back driving mode.

13. The image pickup apparatus according to claim 12, wherein the driven member has a third zone,

wherein the driven member is driven in the second driven zone by the stepping motor in one direction, and after the driven member is driven in the second driven zone, the driven member is driven in the third zone,

wherein in a case where the driven member is driven in the third driven zone, the light shielding member maintains the closed state or the open state, and

wherein in a case where the driven member is driven in the third driven zone, the stepping motor charges the urging member by driving the driven member in the second feed-back driving mode.

14. The image pickup apparatus according to claim 13, wherein after the driven member is driven in the third driven zone and the urging member is charged, the stepping motor holds a current supply.

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